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CHEMICAL MANUFACTURERS ASSOCIATION

2501 M Street, NW 202-887-1100 Washington, D.C. 20037 Telex 89617 (CMA WSH)

BEFORE THE UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

COMMENTS OF THE CHEMICAL MANUFACTURERS ASSOCIATION ON PROPOSED HAZARDOUS ORGANIC NESHAP APPENDICES

National Emission Standards for

Hazardous Air Pollutants for Source
Categories; Organic Hazardous Air
Pollutants from the Synthetic Organic
Chemical Manufacturing Industry and
Seven Other Processes
Fed. Reg. 62608 (Dec. 31, 1992)

A-90-23

Morton L. Mullins Vice President Regulatory Affairs David F. Zoll
Vice President
General Counsel

Karen Fidler Director Air Programs Gary O'Dea Counsel

Of Counsel:

Annette Stanley Manager Air Programs Sonya D. Winner Covington & Burling 1201 Pennsylvania Ave., N.W. P.O. Box 7566

April 19, 1993

Washington, D.C. 20044

Chemical Manufacturers Association 2501 M Street, N.W. Washington, D.C. 20037 (202) 887-1100

LIST OF APPENDICES

APPENDIX Α Applicability for Unit Operations В Total TRI Air Releases For SIC 2865 and 2869 C Evaluation of the Multimedia Impacts on the Hazardous Organic NESHAP D Historical Data Recording for Process Computers E Letter of John Seitz, Director, EPA OAPQS, to Larry Thomas, President, The Society of Plastics F Analysis of Low Flow Cutoff Consistency with TRE Equation G Analysis Supporting Calculation-Based TRE Cutoff for the HON H Letter of Mark Kyjak, Revco Scientific, to Annette Stanley, CMA I Comparison of EPA and CMA Cost Estimates for Large Storage Tanks J Comparison of HON Storage Tank Equations with AP-42 Supplement E K Modeling of Tray-type Steam Stripping **Columns** L Letter of Jan Mayer, EPA OAPOS, to Jerry Schroy, Monsanto company

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Letter of Bruce Davis, Exxon Chemical Company, to Jan Meyer, EPA, OAPQS

Proceedings of the 27th Annual Loss

Process Simulator Comparison

Prevention Symposium

APPENDIX

P	Measurement of Hazardous Air Pollutant Emissions From Wastewater Collection System Components
Q	Comments on Proposed Methods 21, 304 and 305 Contained in the Hazardous Organic NESHAP
R	Fixed Cap Approach Example
S	Letter of CMA to Mr. Rick Colyer, EPA
T	List of Approved EPA Methods

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APPENDIX A

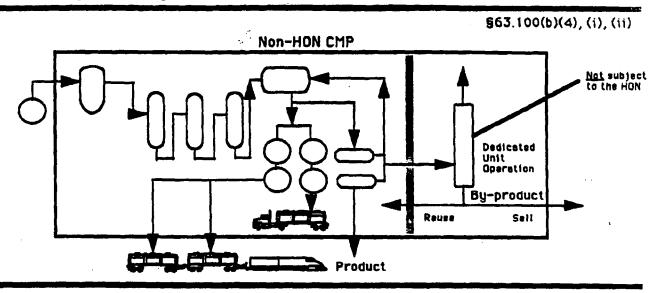
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APPENDIX A

APPLICABILITY FOR UNIT OPERATIONS

Shared Unit Operations, Example 1

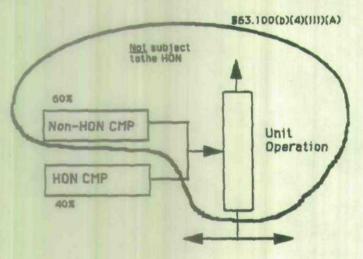
This example represents a unit operation that is dedicated to a non-HON chemical manufacturing process. Even if the unit operation purifies a byproduct, co-product or isolated intermediate stream that is listed in section 63.105 or section 63.184, the unit operation and the non-HON process are not subject to this regulation. This determination would not change if the unit operation was on the front-end or in the middle of the process, as long as it is integral to the chemical manufacturing process.



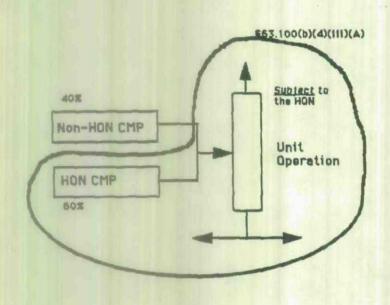
If the same diagram depicted a HON process, then the integral unit operation would be subject to the conditions of the rule.

Shared Unit Operations, Example 2

This unit operation receives its predominant input from a non-HON chemical manufacturing process at the same plant site. In this situation, the unit operation will be associated with the non-HON process even though a portion of its input is from a HON chemical manufacturing process.

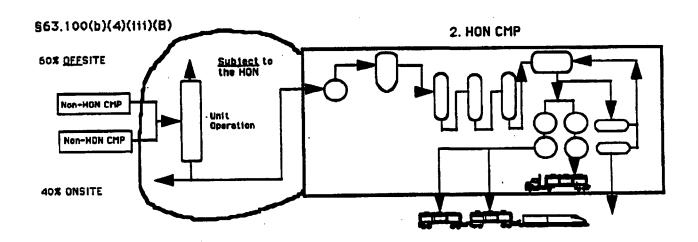


Shared Unit Operations. Example 3
In this situation, the predominant input to the unit operation is from a HON chemical manufacturing process at the same plant site. The unit operation will be associated with the regulated HON process since the predominant need for the unit is due to the input from the HON process.



Shared Unit Operations, Example 4

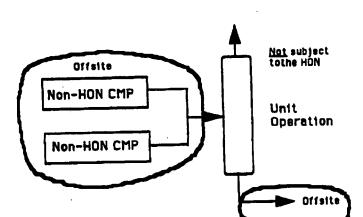
In this situation, the predominant input to the unit operation is from offsite, so the chemical manufacturing process (in this case a HON process) that receives the greatest amount of product from the unit operation would determine the applicability for the unit operation.



Shared Unit Operations, Example 5

In this case, both inputs to the unit operation that are not located at the same plant site and the unit operation does not send its product to a chemical manufacturing process at the same plant site. This type of unit operation would be regulated, if appropriate, as a separate source category.

\$63.100(b)(4)(11)



APPENDIX B

PARHANE

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DBZ	PARHANE	STATE	AKZO CHENICALS INC. CHENICAL DIV. AKZO CHENICALS INC. ALLICO CHENICALS INC. ALLIED-SIGNAL INC. BATDH ROUGE SOUTH ALLIED-SIGNAL INC. BATDH ROUGE SOUTH ALLIED-SIGNAL INC. BATDH ROUGE SOUTH ALLIED-SIGNAL INC. BATHAN ROUGE SOUTH ALLIED-SIGNAL INC. BATHAN ROUGE SOUTH ALLIED-SIGNAL INC. ALTERHATE EMERCY RESOURCES INC. CLIMAX PERFORMANCE MATERIALS CORP. ANERICAN CYANANIO CO. HARNERS PLANT AMERICAN CYANANIO CO. HARNERS PLANT AMERICAN CYANANIO CO. HARNERS PLANT AMERICAN CYANANIO CO. AMERICA	YEAR88	YEAR89	YEAR90
56 57	AKZO CHENICALS INC.	KY	AKZO CHENICALS INC. CHENICAL DIV.	5265	5973	5870
58	AKZO CHENICALS INC.	MA	AKZU CHENICALS INC.	8660	43000	127013 -
59	AKZO CHEMICALS INC.	AL	AKZO CHEMICALS INC.	1729000	1701000	859250
60	AKZO CHEMICALS INC.	MI	AKZO CHENICALS INC.	205050	3767	4231
61	AKZO CHEMICALS INC.	IL	AKZO CHENICALS INC.	357050	338050	485354
63	AKZD CHENICALS INC.	IL	AKZO CHEMICALS INC. NC COOK RESEARCH CENTER	0	2000	775
64	AKZO CHEMICALS INC.	TX	AKZO CHENICALS INC.	230	10650	1300
66	ALLECHENY CHEMICAL CORP.	PA	ALLEGHENY CHENICAL CORP.	9828	0	0300
66 67 68 69	ALLIED COLLOIDS GROUP PLC	VA	ALLIED COLLOIDS INC.	28638	28517	86609
68	ALLIED-SIGNAL INC.	MJ	ALLIED-SIGNAL INC. ELIZABETH	13353	6397	14129
70	ALLIED-SIGNAL INC.	PA	ALLIED-SIGNAL INC.	1458000	1399000	1274005
71	ALLIED-SIGNAL INC.	DE	ALLIED-SIGNAL INC. DELAWARE PLANT	2500	3250	5000
72	ALLIED-SIGNAL INC.	VA	ALLIED-SIGNAL INC. HOPEHELL PLANT	257650	257650	544055
70 71 72 73 74 75 76 77	ALLIED-SIGHAL INC.	OH	ALLIED-SIGNAL INC.	231800	173690	148110
75	ALLIED-SIGNAL INC.	MI	ALLIED-SIGNAL INC.	33858	31396	30032
76	ALLIED-SIGNAL INC.	IL	ALLIED-SIGNAL INC. DANVILLE MORKS	12300	3000	2733
78	ALLIED-SIGNAL INC.	CA	ALLIED-SIGNAL INC.	19731	14164	7245
78 79	ALTERNATE ENERGY RESDURCES INC.	GA	ALTERNATE ENERGY RESOURCES INC.	3204	221	. 0
80 81	ANAX INC.	IL.	CLIMAX PERFORMANCE MATERIALS CORP.	71400	90451	72014
82	AMERICAN CHENICAL SERVICE INC.	IN	AMERICAN CHENICAL SERVICE INC.	21595	18146	8007
83	AMERICAN CYANANID COMPANY	PR	CYANANID AGRICULTURAL DE PR INC.			91300
84 85	AMERICAN CYANANID COMPANY	MJ	AMERICAN CYANANID CO. WARNERS PLANT	8675	7877	1445
86	ANERICAN CYANANID COMPANY	MJ	AMERICAN CYANANID CO. LEDERLE LABORATORIES DIV.	9765	12382	66369
87	AMERICAN CYANANID COMPANY	WV	AMERICAN CYANAMID CO.	1357730	407780	411155
88	AMERICAN CYANANID COMPANY	NE .	AMERICAN CYANAMID CO.	177410	125397	174054
90	ANERICAN CYANANID CUMPANY	MI	AMERICAN CYANAMID CO.	0	0	74200
91	ANERICAN CYAHANID COMPANY	LA	AMERICAN CYANAMID CO. FORTIER PLANT	296750	249100	236855
92 93	ANERSHAN CORP.	IL IL	ANEXTHAN CURP.	1550000	2062100	1281600
94	ANDCO CORP.	AL	ANDCO CHENICAL CO.	2159750	1807670	1972820
95	ANDCO CORP.	MS	ANDCO PETROLEUM ADDITIVES CO.	2249659	2766182	2312496
96 97	ANDCO CORP.	TH	HUNCH CHENICAL CU	4170	6319	3857
98	ANDCO CORP.	: IL	ANDCO CHENICAL: CO.	314350	307750	872650
99	ANDCO CORP.	IL	ANDCO RESEARCH CENTER	22310	22305	23540
100	ANDCO CORP.	TX	ANDCO CHENICAL CO CHOCOLATE RAYOU PLANT	713147	873388	945585
102	ANDCO CORP.	TX	ANDCO CHENICAL CO. TEXAS CITY PLANT A	0	7128	9296
103	ANDCO CORP.	IX	ANDCO CHENICAL CO. TEXAS CITY DOCKS	(42000	149040	122930
104	ANDCO CORP.	TX	ANDCO CHENICAL CO. TEXAS CITY DOCKS ANDCO CHENICAL CO. TEXAS CITY PLANT B	642088	434508	279706
106	ANSPEC CHENICAL CORP	MJ	ANSPEC CHENICAL CORP.	170600	175810	177630
107	ANDERSON DEVELOPMENT CO.	MI	ANDERSON DEVELOPMENT CO.	0	10168	672
108	ANGUS CHEMICAL CO. APPLETON PAPERS INC.	HI	ANGUS CHEMICAL CO.	0	46677	305730
110	APPLIED BIDSYSTEMS	CA	APPLIED BIOSYSTEMS	Ö	1350	1730

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1992 3	YEAR90	1173000	147044 152535 56250	1010200 43870	510 13859	6160 04160	273000 212610	501910 324870 0	261 5900	2504	49901 14183 717	74280 66 700167 182555	1234	1084836 111984 116797 32	0 238662 14	87024 6400	437440 64040 46183 250	537334 35200 14370 51590 21910 15900
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39 FRIDAY.	YEARBB	779000	184652 75950 158250	1226623	2000	5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	640 640 640 640 640 640 640 640 640 640	102257 974645 83327	19603 3511	11700 192231	14050 188500	778465 778465 745177	6476	302369 130756 211504 500	5300 0 127	106469 405213 0	06609	481874 26590 30381 96510 0
TOTAL AIR RELEASES FOR SICS 2865 & 2869 12:39	FACHANE	MISSOURI CHEMICAL MORKS ARCHEM CO.	ARISTECH CHEMICAL CORP. TARBEN PLANT ARISTECH CHEMICAL CORP. ARISTECH CHEMICAL CORP.	ARISTECH CHEMICAL CORP. ARISTECH CHEMICAL CORP. PASADENA ARISTECH CHEMICAL CORP. PASADENA		ASALAND CHEMICAL INC. SOUTH POINT ETHANDL SOUTH POINT ETHANDL		ARCO CHEMICAL CO. BAYFORT DIV. ARCO CHEMICAL CO. BF GOODRICH CO.	BAC PRODUCIS INC. BACKEN CORP. BASE CORP.		:	BAST CORP. COATINGS & COLORANTS DIC. BAST CORP. COATINGS & COLORANTS DIC. BAST CORP.	BRATER HEALTHCARE CORP. BURDICK & JACKSON DIV. RHEIN CHEMIE CORP.	RUGAT CURP. HAARNAKK & REINER CORP. NOGAY CORP. BUSHY PARK PLANT NOGAY CORP.	NILES INC. NOBAY CORP. BEDOUKIAH RESEARCH INC.	HTERNEDIATES FACILITIES	SEC_INTERNEDIATES LA PORTE PLANT BIO-RAD LABORATURIES INC. CHEMICAL DIU. SPECTRUM CHEMICAL MFG. CORP.	BORDEN CHENICAL & PLASTICS BORDEN INC. PACKAGE & INDUSTRIAL PRODUCTS BORDEN PACKAGING & INDUSTRIAL PRODUCTS
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4, 1992	YEAR90	23.4400 23.4400 24.4500 26.04300 26.04300	280745 41719 0 820	136240 30910 255	16176 500 14500 14500	1000 1000 1000 1000 1000 1000 1000 100	15325 15325 1001	1760 18666 184833	124979 12890 15890 8028	1322800 0 151158 19492	3242	3 5 5	221 221 321 043
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12:39 FRIDAY,	YEAR88	1350 1350 1764	626430 81000 500	81265 250 250	230 230 71756 200 200 200 200 200 200 200 200 200 20	1000 1000 1000 1000 1000 1000 1000 100	108378 230 0	19739	7225 0000 0000 0000 0000	1097030 10272 164600 24703	4959 130574 126433 616930	31980 17655 7000 0	28864 1250 750 500 1500
AIR RELEASES FOR SICS 2865 & 2869	FACHANE	BURDEN INC. PACKAGING & INDUSTRIAL PRODS. BURDEN INC. PKG. & INDST. PRODUCTS BURDEN INC. PKG. & INDST. PRODUCTS BURDEN PACKAGING & INDUSTRIAL PRODUCTS BURDEN PACKAGING & INDUSTRIAL PRODUCTS BULDEN SCIENTIFIC CO.	BF CHEMICALS GREEN LAKE BF CHEMICALS GREEN LAKE BROUSSARD CHEMICAL CO.	BIL SPECIALTY RESINS CORP. BIL SPECIALTY RESINS CORP. BURKE CHEMICALS	C. P. Hall CO.	E.P. HANGE GO. HUMPHREY CHENICAL CO. COSAN CHENICAL CONP.	HEIGH CHENCALS INC. CAPITAL RESIN CORP. CARDINAL STABILIZERS INC. CHEM LAB PRODUCTS INC.	CHER SUPPLY CO. CHEMEDESIGN CORP. SPECIALIYCHEN PRODUCTS CORP.	ADVANCED ARDMATICS INC. ADVANCED ARDMATICS INC. AMERICAN TEXNARK INC. DBA TEXNARK CHEMICAL SOLUENTS INC. DEMISON FACILITY CHEMICAL SOLUENTS INC. JENNINGS FACILITY	CHEMINALS INC. PASCAGOULA REFIXERY CHEURDA CHEMINA CO. DAR POINT PLANT CHEURDA CHEMICAL CO.	CHIEF CHENICAL & SUPPLY INC. CIGA-GEIGY CORP. TONS RIVER PLANT CIGA-GEIGY CORP. CIBA-GEIGY CORP. NCINTOSH PLANT CIBA-GEIGY CORP.		SHING COR
TOTAL	STATE	×58855		EX5:	2252:	16522 16522	SENQ:	2£3;	***==	-252 -252	EZGZE:	dexet	25555
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	183	920000000000000000000000000000000000000	727	2212821282	1877	100 100 100 100 100 100 100 100 100 100	7,000	1932	10000	20226	202 204 204 204 204 204	22222 2222 2222 2222 2222 2222 2222 2222	212 214 218 220 220

290	PARHAME	STATE	FACHANE	YEAR88	YEAR89	YEAR90
221 222 223 224 225	CPS CHENICAL CO. CPS CHENICAL CO. CROMPTON & KNOWLES CORP. CROMPTON & KNOWLES CORP. CROMPTON & KNOWLES CORP.	HJ HJ HJ PA	CPS CHEMICAL CO. INC. CROMPTON & KNOWLES CORP. CROMPTON & KNOWLES CORP. CROMPTON & KNOWLES CORP. CROMPTON & KNOWLES CORP. CROWN HITRO INC. DAIGOUR POPE INC. ENVIRONMENTAL PROCESSING INC. DEEPHATER IODIDES INC. JOHN DEERE HORICON WORKS DEGUSSA CORP. ALABAMA GROUP DELTA CHEMICAL CORP. ELECTRONIC MATERIALS DIV. DEXTER CORP. ELECTRONIC MATERIALS DIV. DEXTER CORP. ELECTRONIC MATERIALS DIV. DIAZ CHEMICAL CORP. SUN CHEMICAL CO. INC. ABCO INDUSTRIES LTD. DOUGE CHEMICAL CO. USA MICHIGAN DIV. DOU CHEMICAL CO. LOUISIANA DIV. DOU CHEMICAL CO. LOUISIANA DIV. DOU CORNING CORP. DU PONT OAPE FEAR PLANT DU PONT OLD HICKORY PLANT DU PONT OAPE FEAR PLANT DU PONT HEMPHIS PLANT DU PONT CAPE FEAR PLANT DU PONT TOAPE FEAR PLANT DU PONT TOAPE FEAR PLANT DU PONT HABANDAS CHAMBERS HORKS DU PONT HABANDAS PLANT DU PONT HORIST PLANT DU PONT HABANDAS PLANT DU PONT HABAN	17050 19200 200 1250 55	15170 30558 283 3000 203	15405 44558 642 28 77
226 227 228 229 230	CRONPTON & KNUMLES CORP. CRONPTON & KNUMLES CORP. CROWN HETRO INC. DAICDLOR POPE INC. DAYTON SOFTWATER CORP. INC.	H H H H H H H H H H H H H H H H H H H	CRONPION & KNUMES CORP. CRONPTON & KNOWLES CORP. CROWN METRO INC. DAICOLOR POPE INC. EXVIRONMENTAL PROCESSING INC.	1265 7250 4 1031	766 7000 3	0 1076 6753 10 0 250
231 232 233 234 235	DEEPHATER INC. DEERE & CO. DEGUSSA CORP. DELTA CHENICAL CORP. DELTA FORENOST CHENICAL CORP.	CR UI AL ND TH	DEEPHATER TODIDES INC. JOHN DEERE HORICON WORKS DEGUSSA CORP. ALABANA GROUP DELTA CHENICAL CORP. DELTA FORENOST CHENICAL CORP.	18700 83181 250 1725	10550 62263 23 1690	230 21105 76630 23 1632
236 237 238 239 240	DELTECH CORP DESOTO INC. DEXTER CORP. DEXTER CORP. DIAZ CHENICAL CORP.	LA KH CA KY	DELIECH CORP. DESOTO INC. SPECIALTIES DIV. DEXTER CORP. ELECTRONIC NATERIALS DIV. DEXTER CORP. ELECTRONIC NATERIALS DIV. DIAZ CHENICAL CORP.	23334 33883 0 0 60650	22011 93140 0 41300 93930	45381 0 600 58000 22000 46330
241 242 243 244 245 246	DIC AMERICAS INC. DIC AMERICAS INC. DIC AMERICAS INC. DIC AMERICAS INC. DIXIE CHEMICAL CO. INC.	HI HI TX	SUN CHENICAL CORP. SUN CHENICAL CORP. SUN CHENICAL CORP. SUN CHENICAL CORP. DIXIE PETRO-CHEN INC. DIXIE CHENICAL CO. THE	77000 0 0 0 92753	500 500 0 0 78957	2750 2750 0 0 115480
247 248 249 250 251	DIXIE FURNITURE CO. INC. DODGE CHENICAL CO. DON CHENICAL CO. DON CHENICAL CO. DON CHENICAL CO.	SC MA MI LA	ABCO INDUSTRIES LTD. DODGE CHENICAL CO. DON CHENICAL CO. DON CHENICAL CO. USA MICHIGAN DIV. DON CHENICAL CO. GRAND BAYOU PLANT DON CHENICAL CO. GRAND BAYOU PLANT	5500 1000 1765537 0	6300 1300 1730291 0	8000 1500 1404875 36273 739352
252 253 254 255 256	DOW CHENICAL CO. DOW CHENICAL CO. DOW CORNING CORP DOW CORNING CORP DOW CORNING CORP DU PORT	HY HY HY HY	DON CHENICAL CO. HUGUENOT SITE NICKHEN DON CORNING CORP. DON CORNING CORP. DU PONT CAPE FEAR PLANT	818670 198 741430 525692 3884111	1073830 0 779200 600603 5967210 2913350	925203 0 444000 778380 0
257 258 259 260 261	DU PONT DU PONT DU PONT DU PONT DX SYSTEMS CO	TH TH KY LA TX	DU PONT OLD HICKORY PLANT DU PONT MEMPHIS PLANT DU PONT LOUISVILLE WORKS DU PONT PONTCHARTRAIN WORKS DPC INDUSTRIES INC.	1445208 1377000 677340 352188 5877	2913350 1508500 635870 273597 5000	0 0 0 0
262 263 264 265 266	E. I. DU PONT DE NENDURS INC.	HC HA HA HT	DU PONT GRASSELLI PLANT DU PONT CHANGERS WORKS CHANGERS WORKS DU PONT HIAGARA FALLS PLANT DU PONT GELLE PLANT BELLE PLANT DU PONT HEALING SPRINGS PLANT C & P HEALING SPRINGS	47760 150849 13300 725327 58784	795086 40000	204350 12452 705516 55000
267 268 269 270 271 272	E. I. DU PONT DE NENDURS INC. E. I. DU PONT DE NENDURS INC.	HC AL TX OH NI	DU PONT FAYETTEVILLE PLANT FAYETTEVILLE NORKS DU PONT CAPE FEAR PLANT DU PONT HOBILE PLANT NOBILE PLANT DU PONT OLD HICKORY PLANT DU PONT CAP TOLEDO C & P TOLEDO DU PONT HONTAGENE UNDYS	18023 0 131313 42373	20977 0 19128 0 85488 53582	28975 3384746 16858 1033846 108600 28394
273 274 275	E. I. DU PONT DE HEMOURS INC. E. I. DU PONT DE HEMOURS INC. E. I. DU PONT DE HEMOURS INC.	TX TX TX	DU PORT OLD HICKORY PLANT DU PORT OLD HICKORY PLANT DU PORT CAP TOLEDO C & P TOLEDO DU PORT HORTAGUE HORKS DU PORT LA PORTE PLANT LA PORTE PLANT DU PORT SAGIRE RIVER HORKS SABIRE RIVER HORKS DU PORT GEAUNONT HORKS BEAUNONT HORKS	2570699 884044	1645306 1030180	831644 1711815 925440

DBS	PARMANE	STATE	DU PONT UICTORIA SITE DU PONT CORPUS CHRISTI PLANT CORPUS CHRISTI PLANT CARPENTER CHENICAL CO. CAROLINA EASTHAN CO. TENNESSEE EASTHAN CO. TENNESSEE EASTHAN CO. TEXAS EASTHAN CO. TEXAS EASTHAN CO. EASTON INC. ELAN CHENICAL DISTRIBUTORS INC. ETHYL CORP. ETHYL CORP. ETHYL PETROLEUN ADDITIVES INC. ETHYL PROCESS DEVELOPMENT CENTER ETHYL CORP. ETHYL CORP. ETHYL CORP. ETHYL CORP. ETHYL CORP. EXXON CHENICAL CO. BAYONNE CHENICAL PLANT EXXON CHENICAL CO. TOWAN PRODUCTS EXXON CHENICAL CO. HOUSTON PLANT EXXON CHENICAL CO. BAYTONN OLEFINS FABRICOLOR MEG. CO. FARROUNT CHENICAL CO. INC. FARROUNT CHENICAL CO. INC. FERRO CORP. GRANT CHENICAL DIV. FERRO CORP. FISHER SCIENTIFIC CO. COR PIGNENTS FINC CORP.	YEAR88	YEAR89	YEAR90
276	E. I. DU PONT DE HENOURS INC.	TX.	DU PONT VICTORIA SITE	798817	801070	859961
277	E. R. CARPENTER CO. INC.	TX	CARPENTER CHENICAL CO.	81337	28019	50366
279	EASTNAN KODAK CO.	30	CAROLINA EASTMAN CO.	1467200	1581250	1695800
280 281	FASTMAN KUDAK CU.	AP AP	ADVANCAS FASTNAN CO.	7929934	862737	318537
282	EASTNAN KUDAK CO.	TX	TEXAS EASTMAN CO.	2868602	2656196	1811269
283	EASTON INC.	PR	EASTON INC.	0	2750	. 2700
284 285	EN INDUSTRIES INC	BH	EN SCIENCE	22020	18044	8955
- 286	ENCO CHENICAL DISTRIBUTORS INC	IL	ENCO CHENICAL DISTRIBUTORS INC.	9870	6925	9211
287 288	ETHYL CORP.	20	ETHYL CORP.	775105	35000	350200
289	ETHYL CORP.	LA	ETHYL PROCESS DEVELOPMENT CENTER	48911	53860	93450
290	ETHYL CORP.	AR	ETHYL CORP.	211400	106650	26200
292	ETHYL CORP.	TX	ETHYL CORP. HOUSTON PLANT	82067	43600	36005
293	EXXON	HJ	EXXON CHENICAL CO. BAYONNE CHENICAL PLANT	68	9597	10349
294 295	EXXON	N.I	EXXUN SATURY CHEMICAL PLANT	2831	630	876
296	EXXON	GA	EXXON CHENICAL CALLANAY CHEM. STRANGE PLANT	3841	4711	4786
297	EXXDN	NI	EXXON CHENICAL CO. TONAH PRODUCTS	3820	1414	24910
298 299	FXXIN	LH	FXXIX CHENICAL BOTON POUCE CHENICAL PLANT	510	1487821	1599547
300	EXXON	TX	EXXUN CHENICAL CO. HOUSTON PLANT	53182	55825	67533
301	EXXDX	IX	EXXON CHENICAL CO. BAYTONN OLEFINS PLANT	180100	182500	346440
302	EXXIN CO USA	NJ.	BAYNAY CHEMICAL PLANT (BUCP) (50.20)	113370	96	1000321
304	EXXON CO USA	MJ	LINDEN TECHNOLOGY CENTER	0	661	. 0
305 306	EXXON CORP.	NJ NJ	EXXUN CHENICAL BUTTON BUILDE CHENICAL BLANT	113426	0	0
307	EXXON CORP.	CA	EXXDX CHENICAL CO. BAKERSFIELD BLEND PLANT	1020	ő	ő
308	FABRICOLOR MANUFACTURING CORP.	MJ ·	FABRICOLOR NFG. CO.	0,000	1500	265
309	FAR RESEARCH INC	FL	FAR RESEARCH INC.	3300	313	2192
311	FERRO CORP	OH .	FERRO CORP. BEDFORD CHEMICAL DIV.	128450	52441	39705
312 313	FERRO CORP	IN	FERRO CORP. KEIL CHEMICAL DIV.	2750	124250	1845000
314	FERRO CORP.	LA	FERRO CORP. GRANT CHEMICAL DIV.	29324	0	0
315	FINA DIL & CHENICAL CO.	LA	COSMAR CO.	190601	279586	314572
316 317	FIRMENICH INC.	NJ.	CHEN FLEUR/FIRMENICH	9130	300	3130
318	FIRMENICH INC.	HJ	CHEM-FLEUR/FIRMENICH INC.	0	500	21696
319	FIRST CHEMICAL CORP	PA	QUALITY CHEMICALS INC.	10075	9208	4727
321	FIRST MISSISSIPPI CORP.	MS	FIRST CHENICAL CORP.	143948	98265	50515
322	FISHER SCIENTIFIC CO.	KJ	FISHER SCIENTIFIC CO.	3006	0	0
323 324	FLINT INK CORP. FNC CORP.	HI	CDR PIGNENTS FNC CORP.	0	460	0
325	FMC CORP.	NY.	FMC CORP. MIDDLEPORT PLANT	3402	0	0
326 327	FNC CORP.	MO	FAC CORP.	110060	62988	46303
328	FNC CORP.	MA	FMC CORP. INSTITUTE PLANT FMC CORP. NITRO PLANT	4738	2329	4108
329	FMC CORP.	HC	LITHIUM CORP. OF AMERICA/FMC LITHIUM DIV.	1335	1881	1489
330	FMC CORP.	TX	FMC CORP. BAYPORT PLANT	2108	1975	0

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1992 7	YEAR90	2	4830 1000
DECEMBER 4,	YEAR89	203591 111320 11320 6 9 3 3 0 1140 11320 6 9 3 3 0 1150 0	7030 1587
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TOTAL ATR RELEASES FOR SICS 2865 & 2869 12:39	E FACHANE	INDUSTRIAL CHERICAL PRODUCTS INDUSTRIAL CHERICAL PRODUCTS FREEMAN CHENGAL CORP CHARDUROL DIV. GREENAN CHENGALS CORP CHARDUROL DIV. GREENAN CHENGALS CORP CHARDUROL DIV. GATLIADE CENTICALS CORP. 15P ECHNICALS CORP. 15P ECHNICALS CORP. 16P CHAITCALS CORP. 16C CO. SILLCORP. 16C CORP. 16C CORP	RIZIK
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	Parkane	FRANCE PESSURCE & SUPPLY CO. I FRANCE PESSURCE & SUPPLY CO. I FRANCE PESSURCE S INC. FRANCE PESSURCES PE	. . .
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DBS	PARHANE .	STATE	HENKEL CORP, HENKEL CORP, HENKEL CORP, EMERY GROUP HENKEL CORP. EMERY GROUP HENKEL CORP. CHARLOTTE PLANT HENKEL CORP. CHARLOTTE PLANT HENKEL CORP. HERCULES INC. HUSACH INC. HERCULES INC. HUSACH IN	YEAR88	YEAR89	YEAR90
386	HENKEL CORP.	KJ	HENKEL CORP.	14791	15199	15700
387	HENKEL CORP.	NJ	HENKEL CORP.	34094	34129	33163
388	HENKEL CORP.	PA	HENKEL CORP. ENERY GROUP	0	6768	0
389	HERKEL CORP.	NC 84	MENKEL CORP. ENERY GROUP	177241	205452	106220
391	HENNEL CUDD	CO	HENYEL CORP. CHREUITE PENNI	14000	13600	14400
392	HENKEL CORP.	GA	HENKEL CORP.	60873	69324	44260
393	HERCULES INC.	HJ	HERCULES INC. BURLINGTON PLANT	109040	108420	100750
394	HERCULES INC.	NJ	HERCULES INC.	83600	78100	99000
395	HERCULES INC.	KJ	HERCULES INC.	896228	957860	260
376	HERCULES INC.	VR	MERCULES INC.	1242442	704200	135(20
397	HERCULES INC.	03	HENCHLER THE SPECIALTY CHENTCH'S DIN	118903	139640	54934
399	HERCOLES INC.	CA	HERCULES BRUNSWICK PLANT	2721090	2243164	2072486
400	HERCULES INC.	MS	HERCULES INC.	1016840	723063	684218
401	HEUBACH INC.	KA	HEUBACH INC.	12693	0	0
402	HEXCEL CORP.	NI	HEXCEL CHENICAL PRODUCTS	207650	164450	00000
403	HICKSON DANCHEN CORP	UR	HICKSUN DANCHEN CURP.	0	41273	52232
909	MICH PLAIRS CURP	10	CINCE INDUCTOISE COOP REDNINGHAN FACTIFY	523654	1341125	569749
486	HILLSPORG HOLDINGS CORP	AL	SLOSS INDUSTRIES CORP. ARITON FACILITY	13573	13573	750
407	HILTON DAVIS CO.	SC	HILTON DAVIS CO. COMPENS	0	500	0
408	HILTON DAVIS CO.	NJ	HILTON DAVIS CO. NEWARK	500	500	500
409	HILTON DAVIS CO.	OH	HILTON DAVIS CO. CINCINHATI	644571	73531	45213
410	HOECHRE CELANERE CHEMICAL CKON	IX	HUECHS! CELANESE CHENICAL CROUP INC.	2270121	2514471	150000
412	HULCHEL CELORESE CHEUICHT AKAN	TX	HITCHET CELANESE DANSA PLANT	355640	841800	953105
413	HOECHST CELANESE CORP	RI	HOECHST CELANESE CORP.	23263	35672	39469
414	HOECHST CELANESE CORP	MJ	HOECHST CELANESE HORTHEAST REG. DIST. CENTER	0	0	0
415	HOECHST CELAHESE CORP	MJ	HOECHST CELANESE CHEMICAL GROUP	166162	141305	0
416	HOECHST CELANESE CORP	VR	HOECHST CELANESE CORP.	35845	28005	33703
417	HUECHSI CELAHESE CURP	NG OH	HUTCHET CELANTEE COOR SUIL-TEN	1920	2727	2272
419	HUECHSI CELANESE CORP	HC.	HOFCHST CFLANESE CORP	1030	0	0
420	HOECHST CELANESE CORP	KC	CAPE INDUSTRIES	2985051	2929570	5813399
421	HOECHST CELANESE CORP	AL	HOECHST CELANESE CORP.	257352	246846	249010
422	HOECHST CELAHESE CORP	IL	HOECHST CELANESE CHEMICAL MIDNEST REGIONAL DISTRICT CTR.	42200	0	0
923	HOFCHEL CELVACE COSE	TV	HATCH21 CFUNEZE BELLAKI MAKK2	1224740	1542140	1779770
425	HUECUSI CELANESE CORP	TX	CORPUS CHRISTI TECHNICAL CENTER	28315	2513	10
426	HOLSTON ARMY ANNUNITION PLANT	TH	HOLSTON ARMY AMMUNITION PLANT AMMUNITION PLANT	124200	68000	72636
427	HULS AMERICA INC.	HJ -	HULS AMERICA INC.	5535	5447	2999
428	HULS AMERICA INC.	PA	HULS AMERICA INC. BRISTOL PLANT SITE	0	1000	1255
429	HULS AMERICA INC.	UD	HOTZ BUEKICH CHEZIFKIONN BLANI	20250	9000	49290
430	HULS HIEKICH INC.	W.I	WHART COULD INC	27030	250	10200
432	HUNTSHAN CHENICAL CORP	TX	HUNTSHAN CHENICAL CORP	0	40031	28273
433	HYDRITE CHENICAL CO.	IA	HYDRITE CHENICAL CO.	3254	2682	1159
434	HYDRITE CHEMICAL CO.	MI	HYDRITE CHEMICAL CO.	2050	1661	2137
435	HYDRITE CHEMICAL CO.	MI	HYDRITE CHENICAL CO.	8634	7411	6963
436	HYDRITE CHEMICAL CO.	MI	HIDRITE CHENICAL CU.	4311	1204	752
437	HADDU CAENICAL CO.	PA NI	HYDROL CHENICAL CO.	562	529	640
439	ICC INDUSTRIES INC	OH	ICC INDUSTRIES DOVER CHENICAL CORP	1002	0	. 0
440	ICC INDUSTRIES INC.	OH	ICC INDUSTRIES DOVER CHENICAL CORP.	. 0	503	510
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FRIDAY, DECEMBER	YEAR88 YEAR8	ישרו למואיות ומכו	5	92560 92560 42568 4012 50000 540	45573 48573 48573 7260 41034 16564 16564 16564	38062 18813 198813 13039 13039 15690 6707 5210	572 274 274 5300 28984 28946 18986 16729 16729 250
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TOTAL	STATE	######################################	252226642 250022	STERNOSES STERNOSES	25755722	eguzeess Seuzeess	32225 32225
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DBS	PARNAME	STATE	PELRUN CORP. M & T CHEMICALS INC. ATOCHEM HORTH AMERICA INC. ATOCHEM HORTH AMERICA INC. ATOCHEM MORTH AMERICA INC. FARM & INDUSTRIAL CHEMICAL CO. PERSTORP POLYDLS INC. ALLIAMCE CHEMICAL INC. PFISTER CHEMICAL INC. PHILLIPS & CO. PHILTEX/PYTON COMPLEX PHILLIPS RESEARCH CENTER PHILLIPS & CO. PHILTEX/PYTON COMPLEX ROYAL BOND INC. PIERCE CHEMICALS MORTICIANS SUPPLY PILOT INDUSTRIES OF TEXAS INC. PITMAM-MORRE INC. ALLEMTON PLANT PLASTICS ENGINEERING CO. PLASTICS ENGINEERING CO. PLASTICS ENGINEERING CO. PHASTICS ENGINEERING CO. PHOC SPECIALTIES GROUP CHICAGO PLANT PMC SPECIALTIES GROUP PMC SPECIALTIES GROUP CHICAGO PLANT PMC SPECIALTIES GROUP P	YEAR88	YEAR89	YEAR90
606	PELRON CORP	IL	PELRON CORP.	0	0	0
607	PENNUALI CURP.	NA NO	OTHER MEDIA ONEDICO INC. HOC DEDUTES DIN	1035 47800	1033 6275A	44736
609	PENNHALT CORP.	PA	ATOCHEN N. AMERICA	0	0	20
610	PENNUALT CORP.	AL	ATOCHEN HORTH AMERICA INC.	50712	70934	78638
611	PENNALT CORP.	KY	ATOCHEN NORTH AMERICA INC.	43350	36778	33044
613	PENNUALT COPP	NI	ATTICHEN MURIN MICRICA INC. PIUFRUTEU	13250	5583	6190
614	PENNUALT CORP.	MM	ATOCHEN WORTH AMERICA INC.	1653	2095	2288
615	PENNHALT CORP.	TX	ATOCHEN HORTH AMERICA INC.	7494	2976	3363
616	PENNALT CORP.	IX	ATOCHEN HORIN ANERICA CRUSBY PLANT	18684	3127	3382
618	PENNUALT CORP	CA	FARM & INDUSTRIAL CHEMICAL CO.	1000	0	9120
619	PERSTORP POLYOLS INC.	DH	PERSTORP POLYOLS INC.	6900	6800	7005
620	PFISTER CHEMICAL INC.	HJ	ALLIANCE CHENICAL INC.	8700	6600	3820
621 622	PRISTER CHENICAL INC.	UN UN	PETSTER CHEMICAL INC.	2405	20708	7920
623	PHILLIPS PETROLEUM CO	DK	PHILLIPS RESEARCH CENTER	586	806	5609
624	PHILLIPS PETROLEUN CO	TX	PHILLIPS 66 CO. HOUSTON CHENICAL COMPLEX	73720	36421	110735
625 626	PHILLIPS PETROLEUM CO	TX	PHILLIPS 66 CD. PHILTEX/RYTON COMPLEX	249418	231257	75927
627	PIERCE CHENICAL MODIFICIAN SUPP	TX	PIERCE CHENICALS MORTICIONS SUPPLY	11678	33600	35700
628	PILOT CHENICAL CO.	TX	PILOT INDUSTRIES OF TEXAS INC.	14661	. 18497	9767
629	PITNAM HOURE INC.	PA	PITHAN-HOURE INC. ALLENTOWN PLANT	43400	44217	32213
630	PLASTICS ENGINEERING CO.	MI	PLASTICS ENGINEERING CU.	3725	1404	0
632	PLASTICS ENGINEERING CO.	MI	PLASTICS ENGINEERING CD.	8013	8769	0
633	PMC INC.	NJ.	PNC SPECIALTIES GROUP	8636	8810	8484
634	PMC INC.	OH	PMC SPECIALTIES GROUP	241250	233512	200703
635	PMC INC.	IL	PMC SPECIALTIES GROUP CHICAGO PLANT	1738333	739094	707549
636	PRI THE APPLICATIONS INC	NY	PRI YMED APPLICATIONS THE	364300	04403	Tanono
638	PPG INDUSTRIES INC.	ÜÜ	PPG INDUSTRIES INC.	513150	443090	503055
639	PPG INDUSTRIES INC.	DH	PPG INDUSTRIES INC. BARBERTON PLANT & TECH CTR.	27625	22257	23376
640 641	PPG INDUSTRIES INC.	LA	PPG INDUSTRIES INC.	1785323	1803836	1383029
642	PRESSURE CHENICAL CO	PA	PRESSURE CHENICAL CO.	8516	5528	12265
643	PRIHA INC.	NC	HESTE RESINS CORP.	283971	262300	252600
644	PRIHA INC.	AL	CHEMBOND CORP.	376100	0	0
645	PRING INC.	RL .	WEZIF KEZIWZ COKL.	54279	210019	230582
647	PRIHA INC.	DR	HESTE RESINS CORP.	156850	158100	146700
648	PROCHEM CHEMICALS INC	NC	PROCHEN CHEMICALS INC.	0	250	510
649	PROCTER & GAMBLE	KS	PROCTER & CAMBLE MFG. CO.	1266220'	776206	289280
650 651	PRODUCT-SUL INC	HT NI	DEUCH CHEUICHES	5000	36658	- 17718
652	QUANTUM CHEMICAL CORP.	KJ.	QUANTUM CHENICAL CORP. USI DIV.	500	500	ő
653	QUANTUM CHEMICAL CORP.	IA	QUANTUM CHEMICAL CORP. USI DIV.	344610	191025	116210
654	QUARTUM CHENICAL CORP.	IL	QUANTUM CHEMICAL CORP. USI DIV.	279400	129800	153255
655 656	QUANTUM CHENICAL CORP.	IL	QUANTUM CHEMICAL CORP. USI DIV. TUSCOLA FACILITY QUANTUM - USI TUSCOLA FACILITY	84724	76827	79802
657	QUANTUM CHENICAL COPP.	TX	QUANTUM CHENICAL CORP. USI DIV. DEER PARK PLANT	153787	212819	214190
658	QUANTUM CHENICAL CORP.	CA	QUANTUM CHEMICAL CORP. USI DIV. ANAHEIM PLANT	1500	1000	1000
659	R. B. PANPLIN CORP.	30	MOUNT VERNON MILLS RIECHEN PLANT	1206	5	45
660	R. T. VANDERBILT CO. INC.	CI	VANDERBILT CHENICAL CORP.	1206	158	191

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088.	PARHANE	STATE	VANDERBILT CHEMICAL CORP. R-M INDUSTRIES INC. UNICHEMA MORTH AMERICA RAYCHEN CORP. MORFLEX INC. REILLY INDUSTRIES INC. RHOME PROULENC SPECIALTY CHEMICALS L.P. HOO CHEMICAL CO. INC. RHOME POULENC SPECIALTY CHEMICALS L.P. HOO CHEMICAL CO. INSTITUTE, WU PLANT OPERATION RHOME-POULENC LYMDAL CHEMICALS RHOME-POULENC LYMDAL CHEMICAL CO. RHOME-POULENC LYMDAL CHEMICAL CO. RHOME-POULENC SUFFACTANTS & SPECIALTIES LP RHOME-POULENC BASIC CHEMICAL CO. RHOME-POULENC BASIC CHEMICAL CO. RHOME-POULENC FOR THE WATER TREATMENT CHEMICALS RHOME-POULENC FOR THE WATER TREATMENT CHEMICALS RHOME-POULENC FOR THE WATER TREATMENT CHEMICALS ROHM POULENC FOR THE WATER TREATMENT CHEMICALS ROHM & HAAS DELAMARE VALLEY INC. ROHM & HAAS DELAMARE VALLEY INC. ROHM & HAAS BAYPORT INC. ROHM & HAAS BAYPORT INC. ROHM TECH INC. ROYCE ASSOC. PASSAI COLOR & CHEM. DIV. ROYCE ASSOC. PASSAI COLOR & CHEM. DIV. ROYCE ASSOCIATES PASSAIC COLOR & CHEM. DIV. SACHEN INC. SAM JUAN FIBERGLASS POOLS INC. SACHEN INC. SAM JUAN FIBERGLASS POOLS INC. SACHEN INC. SANDOZ CHEMICALS CORP. MARTIN PLANT SARTOMER CO. INC. CT. SACHENER CO. INC. CT. SACHEMER CO. INC. CT.	YEAR88	YEARBY	YEAR90	
661	R. T. UANDERBILT CO. INC.	KY	UANDERBILT CHENICAL CORP.	409	492	411	
662	R-M INDUSTRIES INC.	ŠČ	R-M INDUSTRIES INC.	1000	1500	42844	
663	RACU FOODS INC.	- IL	UNICHENA KORTH AMERICA	0	0	0	
664	RAYCHEN CORP.	CA	RAYCHEN CORP.	130137	70950	0	
665	REILLY INDUSTRIES INC.	XC	NORFLEX INC.	6489	0	15721	
666	KEILLY INDUSTRIES INC.	NH NH	REILLY INDUSTRIES INC.	71606	76658	79701	
667 668	REILLT IRVUSIKIES IRC.	11	KEILET IRBUSIKIES IRG.	371(0	21721	5/939 n	
669	DEFILY INDUSTRIES INC.	ii.	DEILLY INDUSTRIES INC	1285	51252	41428	
670	REILLY INDUSTRIES INC	ίχ	REILLY INDUSTRIES INC.	4300	84657 31251 0 51353 5000 41023	4300	
671	REILLY INDUSTRIES INC.	ÚŤ	REILLY INDUSTRIES INC.	20477	41023	21838	
672	REXENE CURP.	TX	REXEKE PRODUCTS CO. POLYPROPYLEKE PLAKT	530630	433296	353193	
673	RFS CORP.	NA	ROMA COLOR INC.	31000	1500	140	
674	RHO CHENICAL CO. INC.	IL .	RHO CHENICAL CO. INC.	0	0	10	
675 676	KNURE-PUVLERU IRU. BUNGE-BRINESE INC	#U	KHURE PUULERC SPECIALIT CHENICALS L.P.	186230	213163 106476	8168U 92647	,
677	KRURE-FUULERG IRG. DUNYE-DAMIEYE IYE	PR ND	nsu lu. Duruf-priii fur tiidfartautt 1 toffiai tift	00PG 29A0	10410	1176	
678	RHONE-PROLENC INC	шü	PHONE-POULENC AC CO. INSTITUTE, NV PLANT OPERATIO	MS 88648		22. B	į
679	RHOKE-POULENC INC.	ĜĂ	RHOHE- POULENC LYNDAL CHENICALS	693	729	763	į
680	RHONE-POULENC INC.	FL	RHONE-POULENC POLYPURE WATER TREATMENT CHEMICA	LS 789	28	27	
681	RHONE-POULENC INC.	MO	RHONE-POULENC INC.	0	40800	28420	1
682	RHOKE-POULEKC IKC.	WO	RHONE-POULENC SURFACTANTS & SPECIALTIES LP	2500	1454	1445	!
683	RHONE-POULENC INC.	LA	RHDNE-PUULENC BASIC CHENICAL CO.		100400	4712	
684	KHURE-PUULERU INC.	. 1X	RHURL-PUULLRU IRU. PKELPUKI PLRRI BUNUL-BRUU EUR BRUVBUBE MATER TOPATMENT ENEMSCAL?	70200 0	122400	127883	i
685 686	KNUKE-PUULEKU IKU. BUNUK-BRIII EUR TUR	UM UA	RHUNE-TUVEERC FULITURE WHILK IKEMINER: CHENICHES	970000	221262	20J 429990	i
687	PIUSP HALLSY CHATINES INC	Ti .	PIUFP UNIIFY CRATINCS INC	3,0000	13450	13255	i
688	ROHN A. HAAS CO.	PA	SUPELCO INC	3800	6200	7400	j
689	ROHN &. HAAS CO.	PA	ROHN & HAAS DELAWARE VALLEY INC.	313603	252952	247226	,
690	ROHN A. HAAS CO.	PA	RUHN & HAAS DUI PHILADELPHIA PLANT	258755	248189	206421	,
691	ROHN &. HAAS CO.	TH	ROHN & HAAS INC. TENNESSEE	27880	38510	40720	į
692	RUHN &. HAAS CO.	IX	RUHN & HRAS INC. TEXAS	2288762	1816423	832088	
693 694	KUNA L. HARS CU. BAUM TECU INC	AN AM	KUNN & KAHS BRITURI INC. BNUM TERU INC	742 9000	10097	137 4900	
695	DUALL TECH. TUP.	N.S	PHYTE ACCULATE THE PACCAL CHEM ALL	7900	17031	OUEF .	1
696	ROYCE ASSOCIATES ALP	йJ	ROYCE ASSOCIATES PASSAIC COLOR & CHEM. DIV.	ŏ	ď	Ŏ	į
697	RPN INC.	ÖÄ	EUCLID CHENICAL CD.	10345	28	· Õ	}
698	RSA CORP.	HY	RSA CORP.	5550	4150	2850	į
699	RUETGERS-HEASE CHEMICAL CO. IK	PA	RUETGERS-HEASE CHENICAL CO. INC.	13741	0	0	!
700	RUETGERS-NEASE CHEMICAL CO. IN	GA -	RUETGERS-NEASE CHENICAL CO. INC.	320	, 600	790	1
701 702	KULISEKS-MERSE CHENICAL CU. IM	UM	KULIBEKS-RERSE CHENICHE EU. IKU.	23500	Ü	1122	J
703	TAN HAN CIRCULATE DADIE INC	10	TAN MAN ETREDELATE DAME THE	24000	ŭ	132	i
704	SANDOZ CHENICAIS COPP	i.k	SANDOT CHENICALS COOP FAIR LAUN	5020	4900	1555	Ĺ
705	SANDOZ CHEMICALS CORP	ÄČ	SANDOZ CHENICALS CORP. MT. HOLLY PLANT	40415	9900	12963	i
706	SANDUZ CHENICALS CORP.	2C	SANDOZ CHENICALS CORP. MARTIN PLANT	8770	4403	2370	į
707	SARTUHER CO. INC. UC	CT	SARTONER-GO. INC. CT.	3757	5333	5325	į
708	SARTOMER CO. INC. NC SCHENECTADY CHEMICALS INC	PA	SANDOZ CHEMICALS CORP. MT. HOLLY PLANT SANDOZ CHEMICALS CORP. MARTIN PLANT SARTONER-GO. INC. CT. SARTONER CO. INC. NC SCHENECTADY CHEMICALS INC. SCHENECTADY CHEMICALS INC. SCHEN CHEMICALS INC. SCHER CHEMICALS INC. SCHER CHEMICALS INC. SCHER CHEMICALS ORP	_84434	45762	44994	1
709	2CHENECIADY CHEMICALS INC	МĀ	SCHENECTARY CHEMICALS INC.	500389	462497	425797	,
710 711	SCHEHECTADY CHEMICALS INC	1 A M.1	SCHERELIHUT CHERICHES INC.	5060 500	5420 500	25256 0	
711 712	SCHER CHEMICALS INC.	TI	SUFFICE CHEMICAL INC.	821730		327985	
713	SCHERING CORP. SEADDARD CHENICAL CORP.	ÄČ	SCHENECTADY CHEMICALS INC. SCHENECTADY CHEMICALS INC. SCHER CHEMICALS INC. SCHER CHEMICALS INC. SHEREX CHEMICAL CO. INC. SEABOARD CHEMICAL CORP.	38654	000070	321703	
714	SEQUA CORP.	2 <u>C</u>	SEDILO CHENICALS INC	7195	6607	9288	j
715	SHELL DIL CO.	LA	SHELL DIL CO. HORCO MFG. COMPLEX	588010		609560	į
				•			

082	PARNAME	STATE	SHELL OIL CO. HORCO NFG. COMPLEX - MEST SHELL CHEMICAL CO. GEISMAR PLANT SHELL OIL CO. DEER PARK NFG. COMPLEX SHELL OIL CO. MARTIMEZ MANUFACTURING COMPLEX SHEPHERD CHEMICAL CO. SHEPHERD CHEMICAL CO. BUFFALO COLOR CORP. SHIPLEY CO. INC. KESSHAN & BOST CHEMICAL CO. INC. ALDRICH CHEMICAL CO. INC. ALDRICH CHEMICAL CO. INC. ALDRICH CHEMICAL CO. INC. SIGMA CHEMICAL CO. INC. SIGMA CHEMICAL CO. INC. SIGMA CHEMICAL CO. SILWENT MANUFACTURING CO. INC. SOLVENT MANUFACTURING CO. INC. SOLVENTS & CHEMICALS INC. STEPAN CO. STEPAN CO. MILLSDALE PLANT STERLING CHEMICALS INC. STEPAN CO. MIRTHEST PEROCHEMICAL CORP. STOCKHAUSEN INC. STOKKHAUSEN INC. TEXACO CHENICAL CO. PORT ARTHUR CHENICAL PLANT TEXACO CHENICAL CO. TEXACO CHENICAL CO. TEXACO CHENICAL CO. TEXACO CHENICAL CO. TEXAS ALKYLS INC. TEXACO CHENICAL CO. TEXAS PEROCHENICALS CORP. ESSEX INDUSTRILAL CHENICALS INC. DOM CHEMICAL CO. GRAND BAYOU PLANT TOURER CHEMICAL CORP. CEOAR CHENICAL CORP. CEOAR CHEMICAL CORP. TOURER CHEMICAL CORP.	YEAR88	YEAR89	YEAR90
716 717	SHELL DIL CO.	LA	SHELL DIL CO. HORCO NFG. COMPLEX - WEST SHELL CHEMICAL CO. GEISMAR PLANT	1593500	1328420	226220 977526
718 719	SHELL DIL CO.	CA	SHELL DIL CO. DEER PARK NFG. COMPLEX SHELL DIL CO. MARTINEZ MANUFACTURING COMPLEX	1464450 65707	3498072 66070	2953088 97008
720 721	SHERBORNE GROUP INC.	NY NA	SHEPHERD CHENICAL CU. BUFFALO COLOR CORP.	114846	274501	270475
723	SHO CHEM INC. SIGNA-ALDRICH CORP.	XT	KEESHAN & BOST CHEMICAL CO. INC. ALDRICH CHEMICAL CO. INC.	1000	1500 750	1000
725 726	SIGNA-ALDRICH CURP.	IN	ALDRICH CHENICAL CO. INC.	1468	750 1467	1250 1532
722 723 724 725 726 727 728 729	SIGNA-ALDRICH CORP.	MI .	SIGNA CHENICAL CO.	4088	750 22289	1510
730 731	SINCLAIR & VALENTINE L. P.	PA	RIDGHAY COLOR CO. SOLVENT NAMUFACTURING CO. INC.	0	250	0
732 733	SOLVENTS & CHEMICALS INC. SOUTHWESTERN ANALYTICAL CHEMIC	TX	SOLVENTS & CHEMICALS INC. SACHEM INC. CHEMICALS INC.	5976 143	466	8957 732
734 735 736	STEPAN CO.	IL TY	STEPAN CO. NILLSDALE PLANT	481453	333774 653540	337270 719860
737	STINSON LUNBER CO. STOCKHAUSEN INC.	WA	HORTHWEST PETROCHEMICAL CORP. STOCKHAUSEN INC.	1000	7450	1000
739	STORER INC. SURBELT CORP.	PA	STONER INC. SUNBELT CORP.	2250 250	2500 250	1750 250
741 742 743	SYBRON CHENICALS INC.	20,	SYBRUN CHENICALS INC. SYBRUN CHENICALS INC.	1000	500	8762 63
744 745	SYNALLOY CORP. SYNTEX AGRIBUSINESS INC.	SA MD	BLACKMAN UHLER CHEMICAL DIV AUGUSTA CHEM. FACILITY SYNTEX AGRIBUSINESS INC.	1571027	2158330	5800 2024302
746	TANA CHENICALS CO LTD TECH SPRAY INC	TX	HOSES LAKE INDUSTRIES TECH SPRAY INC.	0	250 3500	3500 1350
748 749 750	TELEDYNE NCCORNICK SELPH	CA TN	TELEDYNE NCCORNICK SELPH TENNESSEE UNLIFY PERFORMANCE PRODUCTS INC	13978	24943	164363
751 752	TEXACO INC. TEXACO INC.	KS	TEXACO REFINING & MARKETING INC. EL DORADO PLANT TEXACO CHENICAL CO.	1145880 63162	1167311 55320	1152380 50813
753 754	TEXACO INC.	IX	TEXACO CHENICAL CO. PORT ARTHUR CHENICAL PLANT TEXACO CHENICAL CO.	433250 954202	484300 707080	274611 626360
755 756 757	TEXAS ALKYLS INC.	TX	TEXAS ALKYLS INC. TEXAS PETROCHENICALS CORP	9150 228337	11987	9696 251081
758 759	THE DOW CHEMICAL CO	ND LA	ESSEX INDUSTRIAL CHEMICALS INC. DON CHEMICAL CO. GRAND BAYOU PLANT	1829 673	32319	0
760 761 762	THE QUAKER DATS CO TOWER CHENICAL CORP. TRANS RESOURCES INC.	PA AR	TOWER CHENICAL CORP.	4000	2000	25 3010
763 764		PA SC	CEDAR CHENICAL CORP. FEDERAL LABORATORIES PYRO DIV. TRAYLOR INC.	29100	27516 1000	34900
765	UNION CAMP CORP. UNION CAMP CORP.	FL	UNION CAMP CORP. BBA DIV. ALT CHEMICALS	101205	66993 24425	39157 38208 419954
767 768 769	UNION CARBIDE CORP UNION CARBIDE CORP UNION CARBIDE CORP	MA MA	UNION CARBIDE C & P CO. INSTITUTE NV PLANT OPERATIONS UNION CARBIDE CHENICALS & PLASTICS CO. HOLZ IMPOUNDMENT UNION CARBIDE CORP. TECHNICAL CENTER	441508 0 11672	382268 1971 8450	2774 560
770	UNION CARBIDE CORP	ÜŬ	UNION CARBIDE CHEMICALS & PLASTICS CO. INC.	1119859	805323	170181

0B2	PARHAME	STATE	UNION CARBIDE CHEMICALS & PLASTICS CO. INC. UNION CARBIDE CORP. STAR PLANT UNION CARBIDE INDUSTRIAL CHEMICALS AMERCHOL CORP. UNION CARBIDE CHEMICALS & PLASTICS CO. MARINE TERMINAL UNION CARBIDE CHEMICALS & PLASTICS CO. SEADRIFT PLANT UNION CARBIDE CHEMICALS PLASTICS CO. SEADRIFT PLANT UNION CARBIDE CHEMICALS PLASTICS CO. SEADRIFT PLANT UNION OIL OF CALIFORNIA DBA UNCOAL UNION TEXAS PRODUCTS CORP. GEISMAR ETHYLEHE PLANT UNIRTYAL CHEMICAL CO. INC. UNIRTYAL CHEMICAL CO. INC. UNIRTYAL CHEMICAL CO. INC. UNITEX CHEMICAL CORP. UNITEX CHEMICAL CORP. UNITEX CHEMICAL CORP. UNION SUREUEPORT PLANT UPJOHN CO. FINE CHEMICAL DIU. UNANDEMARK CHEMICAL CORP. UELSICOL CHEMICAL CORP. UELSICOL CHEMICAL CORP. ULISTA CHEMICAL CORP. UNISTA CHEMICAL CORP. UNISTA CHEMICAL CO. LAKE CHARLES CHEMICAL COMPLEX UNICAN CHEMICAL CO. UNISTA CHEMICAL CO. LAKE CHARLES CHEMICAL COMPLEX UNICAN CHEMICAL CO. UNISTA CHEMICAL DIU. UNICO CORP. HUMNO CHEMICAL DIU. UNICO CORP. ARGUS CHEMICAL DIU. UNICO CORP. ARGUS CHEMICAL DIU. UNICO CORP. ORGANICS DIU. UNICO CORP. UNICO CORP. ORGANICS DIU. UNICO CORP.	YEAR88	YEAR89	YEARPO
771	UNION CARBIDE CORP	uv .	UNION CARBIDE CHENICALS & PLASTICS CO. INC.	689963	728806	868871
773	UNION CARBIDE CORP	LA LA	UNION CARBIDE CURP. SIRK PERRI UNION CARBIDE INDUSTRIAL CHEMICALS	335223	ប 0	68333 202900
774	UNION CARBIDE CORP	LA	AMERCHOL CORP.	572	572	572
775 776	UNION CARBIDE CORP	IX TY	UNION CARBIDE CHEMICALS & PERSIICS CO. MARINE TERMINAL	145317	E21661	161145 73398
777	UNION CARBIDE CORP	ŤΧ	UNION CARBIDE CHEMICALS PLASTICS CO. SEADRIFT PLANT	1154243	1199998	940807
778	UNIDH OIL CO	TX	UNION DIL OF CALIFORNIA DBA UNDCAL	184662	459310	0
779 200	INTERNATION CREATCH CU TAC	LA	UNION IEXAS PRODUCIS CORP. GEISTAR EINTLERE PLARI	UCUPE 14129	11620U 99978	12936U 25910
781.	UNIRDYAL CHEMICAL CO INC	ŬĤ	UNIRDYAL CHENICAL CO. INC.	119003	73500	64618
782	UNIRUYAL CHEMICAL CO INC	LA	UNIRDYAL CHEMICAL CO. INC.	220423	374215	265310
783 704	UNITED ORGANICS CORP	, MC	UNITED ORGANICS CORP.	104570	9630 46794	01 QAQ
785	UNP	IL	UNP	91301	51862	49338
786	ÜÜP	ĹŘ	UOP SHREVEPORT PLANT	11250	4900	3450
787	UPJOHK CO.	CI	UPJOHN CO. FINE CHEMICAL DIV.	70430	37313	20000
789	UFISIONI CHENICAL COURC	TH	UFLSICAL CHENICAL CORP	370834	383170	289581
790	VELSICOL CHENICAL CORP.	TH	VELSICOL CHENICAL CORP.	275589	163240	49978
791	VELSICOL CHENICAL CORP.	ĬĹ	VELSICOL CHENICAL CORP.	552	2710	A150
792	VININGS INDUSTRIES INC.	ND .	VIRINGS INVUSIRIES INC. UISTO CHENICAL CO	976BB	02334 02333	65288
794	VISTA CHENICAL CO.	HS	UISTA POLYNERS INC. UISTA POLYNERS DIV.	76812	76712	63993
795	UISTA CHENICAL CO.	LA .	VISTA CHENICAL CO. LAKE CHARLES CHENICAL COMPLEX	671700	630713	581338
796 797	UULCAN ARIERIALS CUMPARY	NH K2	U D CDACE 1 CO - CONN OPCANIC CHEMICALS DIN	1130838 7504	8464	320307
798	W. R. GRACE & CO.	ŤΧ	W. R. GRACE & CO. DEER PARK FACILITY	81338	71825	15334
799	HACKER SILICONES CORP.	HI	WACKER SILICONES CORP.	8700	9650	9403
800 201	NRKU CHEMICALS USA INC.	UA AU	NAKU CHENICRES USA INC. UBRUINCTON CUCNICAL INC	ีย ก		UPGP 24
802	WERKER C. SMITH INC.	ÖÄ	WERKER C. SHITH INC.	· ŏ	30 0	50ŏ
803	HESTERN TAR PRODUCTS CORP.	TH-	HESTERN TAR PRODUCTS CORP.	1500	1000	500
804 905	WESTERN TAR PRODUCTS CORP.	IX	NESTERN TAR PRODUCTS CORP.	2300 1994	3/UU 2011	1300
-808	WITCO CORP	ίκ	WITCO CORP. HUNKO CHENICAL DIV.	1480	405	275
807	WITCO CORP.	HJ	HITCO CORP. ORCANICS DIV.	3909	3872	5637
808	WITCO CORP.	M?	NITCO CORP. ARGUS DIV.	C88E	6184 9200	. 406 . 406
810	WITCO CORP	ŤŔ	WITCO CORP. HUNKO CHENICAL DIV.	10058	47291	16224
811	WITCO CORP.	ĬĹ	WITCO CORP.	30935	16536	10452
812	WITCO CORP.	LR	NITED CORP. ARGUS CHERICAL DIV.	3378	16944	15827
814	WIICO CORP.	TX	WITCO CORP	4163	2320	2310
815	UITCO CORP.	. ČŘ	HITCO CORP. ORGANICS DIV.	235	951	2005
816	WITCO-CORP.	CA	U. J. PERDXYSEX	08P	() *1229	0 974779
818 ATL	NKIONI UNENIUHE CURP. ZALCON INC	RC DH	AKIONI TUKNITHE FORF. ZACLON INC	027273	Portor	317113
819	ZIEGLER CO. INC.	üï	NASTE RESEARCH & RECLANATION CO. INC.	20998	Õ	Ŏ
				14387555	12353525	88833838 194677909
				*45641167		EUE I IUFUA

§63.183 List of volatile hazardous air pollutants.

	
CHEMICAL NAME	CAS NUMBER
Acetaldehyde	75070
Acetamide	60355
Acetonitrile	75058
Acetophenone	98862
2-Acetylaminofluorine	53963
Acrolein	107028
Acrylamide	79061
Acrylic acid	79107
Acrylonitrile	107131
Allyl chloride	107051
4-Aminobiphenyl	92671
Aniline	62533
o-Anisidine	90040
Benzene	71432 ·
Benzidine	92875
Benzotrichloride	98077
Benzyl chloride	100447
Biphenyl	92524
Bis(2-ethylhexyl)phthalate	(DEHP) 117817
Bis(chloromethy1)ether	542881
Bromoform	75252
1,3-Butadiene	106990
Caprolactam	105602
Carbon disulfide	75150
Carbon tetrachloride	56235
Carbonyl sulfide	463581
Catechol®	120809
Chloroacetic acid	79118
2-Chloroacetophenone	532274
Chlorobenzene	108907
Chloroform	67663
Chloromethyl methyl ether	107302
Chloroprene	126998
-	

Cresols and cresylic acids (mixed)	1319773
Cresol and cresylic acid (o-isomer)	95487
Cresol and cresylic acid (m-isomer)	108394
Cresol and cresylic acid (p-isomer)	106445
Cumene	98828
2.4-D, salts and esters	94757
DDE	3547044
Diazomethane	334883
Dibenzofurans	132649
1,2-Dibromo-3-chloropropane	96128
Dibutylphthalate	84742
1,4-Dichlorobenzene(p-)	106467
3,3'-Dichlorobenzidine	91941
Dichloroethyl ether (bis(2-chloroethyl)ether)	111444
1,3-Dichloropropene	542756
Diethanolamine	111422
N, N-Dimethylaniline	121697
Diethyl sulfate	64675
3,3'-Dimethoxybenzidine	119904
Dimethyl aminoazobenzene	60117
3,3'-Dimethylbenzidine	119937
Dimethyl carbamoyl chloride	79447
Dimethylformamide	68122
1,1-Dimethylhydrazine	57147
Dimethyl phthalate	131113
Dimethyl sulfate	77781
4,6-Dinitro-o-cresol, and salts	534521
2,4-Dinitrophenol	51285
2,4-Dinitrotoluene	121142
1,4-Dioxane (1,4-Diethyleneoxide)	123911
1,2-Diphenylhydrazine	122667
Epichlorohydrin (1-Chloro-2,3-epoxypropane)	106898
1,2-Epoxybutane	106887
Ethyl acrylate	140885
Ethylbenzene	100414

Ethyl carbamate (Urethame)	51796
Ethyl chloride (Chlorecthane)	75003
Ethylene dibromide (Debromoethane)	106934
Ethylene dichloride (1,2-Dichloroethane)	107062
Ethylene glycol	107211
Ethylene oxide	75218
Ethylene thiourea	96457
Ethylidene dichloride (1,1-Dichloroethane)	75343
Formaldehyde	50000
Glycol ethers ^a	0
Hexachlorobenzene	118741
Hexachlorobutadiene	87683
Hexachloroethane	67721
Hexamethylene-1,6-diis@cyanate	822060
Hexamethylphosphoramide	680319
Hexane	110543
Hydrazine	302012
Hydroquinone	123319
Isophorone	78591
Maleic anhydride	108316
Methano1	67561
Methyl bromide (Bromomethane)	74839
Methyl chloride (Chloromethame)	74873
Methyl chloroform (1,1,1-Tri@hloroethane)	71556
Methyl ethyl ketone (2 - Butanome)	78933
Methyl hydrazine	60344
Methyl iodide (Iodomethane)	74884
Methyl isobutyl ketone (Hexone)	108101
Methyl isocyanate	624839
Methyl methacrylate	80626
Methyl tert butyl ether	1634044
4,4-Methylene bis(2-chloroaniline)	101144
Methylene chloride (Dichloromethane)	75092
Methylene diphenyl diisocyanaste (MDI)	101688
4,4'-Methylenedianiline	101779

Naphthalene	91203
Nitrobenzene .	98953
4-Nitrobiphenyl	92933
4-Nitrophenol	100027
2-Nitropropane	79469
N-Nitroso-N-methylurea	684935
N-Nitrosodimethylamine	62759
N-Nitrosomorpholine	59892
Phenol .	108952
p-Phenylenediamine	106503
Phosgene	75445
Phthalic anhydride	85449
Polychlorinated biphenyls (Aroclors)	1336363
1,3-Propane sultone	1120714
beta-Propiolactone	57578
Propionaldehyde	123386
Propoxur (Baygon)	114261
Propylene dichloride (1,2-Dichloropropane)	78875
Propylene oxide	75569
1,2-Propylenimine (2-Methyl aziridine)	75558
Quinone	106514
Styrene	100425
Styrene oxide	96093
2,3,7,8-Tetrachlorodibenzo-p-dioxin	1746016
1,1,2,2-Tetrachloroethane	79345
Tetrachloroethylene (Perchloroethylene)	127184
Toluene	108883
2,4-Toluene diamine	95807
2,4-Toluene diisocyanate	584849
o-Toluidine	95534
1,2,4-Trichlorobenzene	120821
1,1,2-Trichloroethane	79005
Trichloroethylene	79016
2,4,5-Trichlorophenol	95954
2,4,6-Trichlorophenol	88062

	\mathbf{v}

Triethylamine	121448
Trifluralin	1582098
2,2,4-Trimethylpentame	540841
Vinyl acetate	108054
Vinyl bromide	593602
Vinyl chloride	75014
Vinylidene chloride (1,1-Dichloroethylene)	75354
Xylenes (not otherwise specified)	1330207
Xylene (o-isomer)	95476
Xylene (m-isomer)	108383
<pre>Xylene (p-isomer)</pre>	106423

APPENDIX C

APPENDIX C

EVALUATION OF THE MULTIMEDIA IMPACTS OF THE HAZARDOUS ORGANIC NESHAP (HON)

for:

Chemical Manufacturers Association 2501 M Street, NW Washington, D.C. 20037

by:

Environmental Quality Management, Inc. 1310 Kemper Meadow Drive Cincinnati, Ohio 45240

CONTENTS

	<u>Page</u>
TABLES	iii
1. INTRODUCTION	1
2. REGULATORY REVIEW AND IDENTIFICATION OF MULTIMEDIA IMPACTS	3
2.1 SUMMARY OF NOx AND CO REGULATIONS	3
2.2 EMISSION RATES	4
2.3 NEW SOURCE REVIEW IMPACTS	5
2.4 NOx AND CO REGULATORY IMPACTS FOR MODEL PLANTS	7
3. IMPACT EVALUATION FOR HALOGENATED STREAMS	8
4. COST-EFFECTIVENESS OF NOx CONTROL	9
5. CONCLUSIONS	11

TABLES

Number	<u>Page</u>
1. STATES COMPRISING 90 PERCENT OF THE SOCMI CAPACITY	12
2. SUMMARY OF NONATTAINMENT AREAS BY STATE	13
3. MODEL PLANT PARAMETERS FOR THE HON SOURCE CATEGORIES	20
4. SECONDARY IMPACTS FOR INCINERATION CONTROL OF CMA MODEL PROCESS VENT STREAMS	21
5. SECONDARY IMPACTS FOR INCINERATION CONTROL OF EPA MODEL PROCESSIVENT STREAMS	22
6. ELECTRICAL ENERGY REQUIREMENTS AND S02 EMISSION RATES FOR THE EROCESS VENT MODEL PLANTS	23
7. SECONDARY EMPACTS FOR ENCINERATION CONTROL OF EPA MODEL LOADING RACK STREAMS	24
8. SECONDARY IMPACTS FOR STREAM STRIPPER CONTROL OF EPA MODEL WASTEWATER STREAMS	27
9. SUMMARY OF MAJOR NEW SOURCE REVIEW APPLICABILITY CRITERIA	28
10. SUMMARY OF REGULATORY APPLICABILITY FOR EXISTING MINOR SOURCE	29
11. SUMMARY OF REGULATORY APPLICABILITY FOR EXISTING MAJOR SOURCE	30
12. SCRUBBER WATER RATES	31
13. NOx CONTROL COST-EFFECTIVENESS FOR THERMAL OXIDIZER SYSTEMS.	32

SECTION 1 INTRODUCTION

On December 31, 1992, U. S. Environmental Protection Agency (EPA) published a proposed rule in the <u>Federal Register</u> for regulating the emissions of certain organic hazardous air pollutants from synthetic organic chemical manufacturing industry (SOCMI) production processes which are part of major sources under Section 112 of the Clean Air Act. The proposed rule, referred to as the hazardous organic NESHAP or the HON, would require implementation of control measures that are defined as maximum achievable control technology (MACT) for certain sources. Five source types in the SOCMI are affected by the proposed rule; these are:

- Storage tanks
- Process vents
- Equipment leaks
- Wastewater collection and treatment operations
- Transfer loading operations

With the exception of the equipment leaks source category, the proposed rule requires add-on controls for the affected sources. The background information document (BID) for the proposed HON rule provides the basis and performs impacts assessment for the affected sources.

Environmental Quality Management, Inc. (EQ) has been contracted by the Chemical Manufacturers Association (CMA) to evaluate the multimedia impacts of the HON for the SOCMI source categories. The project scope consists of examining the BID to understand and critique EPA's basis and assumptions in its evaluation of multimedia impacts, and quantifying multimedia impacts for the affected source categories.

This report documents the methodology and multimedia impacts of the proposed HON regulations. The analysis addresses the source categories of process vents, transfer and loading operations, and wastewater collection and treatment operations. The reference control technology (RCT) for the storage tank source category consists of floating roof related technology that does not generate secondary emissions, and thus it is not included in the analysis. The ap-

proach used for the evaluation of the multimedia impacts along with the source sizes used as a basis for evaluation is presented and impacts of the RCT identified by EPA are presented. Section 2 of the report provides the regulations overview and identifies the NOx and CO impacts for the model plants. Section 3 identifies the multimedia impacts associated with the halogenated gas streams. The cost-effectiveness of controlling NOx emissions from the thermal oxidizer systems is discussed in Section 4. The study conclusions are presented in Section 5.

SECTION 2

REGULATORY REVIEW AND IDENTIFICATION OF MULTIMEDIA IMPACTS

Multimedia impacts associated with the RCTs for three HON source categories (process vents, transfer and loading operations, and wastewater collection and treatment operations) are discussed in this report. These source categories require installation of add-on control systems that generate emissions of nitrogen oxides (NOx) and carbon monoxide (CO). The MACT for the process vents and transfer and loading operations has been defined as installation of thermal oxidizer systems. The MACT for the wastewater collection and treatment operations has been defined as installation of steam stripper system. The NOx and CO emissions are regulated by EPA and the states where SOCMI plants are located. Any increase in the NOx and CO emissions must be analyzed for their regulatory impacts. This analysis identifies the regulations that must be complied with and quantifies the NOx and CO emissions for the model plant sizes defined by CMA and EPA.

2.1 SUMMARY OF NOx AND CO REGULATIONS

The review of the geographic distribution of the SOCMI process units indicates that 17 states account for 90 percent of the total SOCMI process units in the United States. Table 1, based on the data available in the BID, indicates the states that comprise 90 percent of the SOCMI process unit capacity. The regulatory evaluation of the NOx and CO emissions for the three SOCMI source categories was performed for the 17 states identified in Table 1.

Table 2 identifies the CO, NOx, and ozone nonattainment areas for the 17 states listed in Table 1. No areas in the 17 states are currently identified as nonattainment for NOx, however, the NOx emissions will be covered under ozone attainment status since NOx has been identified as a precursor to ozone. The definition of the nonattainment areas is based on the Clean Air Act (CAA) amended on November 15, 1990. The CAA specifies design values for ozone and deadlines for attaining the ozone standards.

2.2 EMISSION RATES

To facilitate the evaluation of the multimedia impacts, model plants were defined for each of the three source categories. Table 3 shows the model plant parameters used for evaluating the multimedia impacts.

NOx and CO emission rates were estimated for the model plants identified in Table 3. The NOx emission rates for the incineration systems were based on a NOx concentration of 150 ppm in the exhaust stream. EQ contacted burner manufacturers and reviewed in-house data to determine the representative NOx concentration for the exhaust streams controlled by incinerators. The NOx concentration depends upon the type of burner and also varies from manufacturer to manufacturer. Regulation of NOx by EPA has lead to design of low NOx burners by manufacturers. NOx levels under 100 ppm can be achieved by the current burner designs. Some vendors can guarantee NOx levels under 50 ppm. The CO emissions were based on the data available in the BID.

For the process vent model plants, SO₂ emission rates associated with the electrical energy requirement were also calculated. Electrical energy requirement for the model plants was based on a system pressure drop of 20 inches of water and annual operating hours of 8760. A heat rate of 10,000 Btu/kWh was used to estimate the coal consumption associated with the electrical energy required to operate the incinerator system. The annual SO₂ emissions were based on a SO₂ emission rate of 1.2 lb/10⁶ Btu heat input. These parameters formed the basis for evaluation of the regulatory impacts.

Table 4 shows the NOx and CO emission rates for the 4 process vent model plants defined by CMA. The NOx and CO emission rates for the 12 model plants included in the BID were also calculated and are summarized in Table 5. The SO2 emission rates associated with the electrical energy required to operate the incinerator are shown in Table 6.

Table 7 summarizes the secondary impacts for the model loading racks streams. The secondary impacts for the wastewater model plants are summarized in Table 8.

2.3 NEW SOURCE REVIEW IMPACTS

Plants which choose to install incineration to satisfy RCT requirements for affected process vents may be faced with additional regulatory requirements for permitting under CAA Title I, Parts C and D. Part C, Title I provides requirements for new source review (NSR) for major sources located in attainment areas. The implementing regulations are provided at 40 CFR 52.21, and are commonly referred to as Prevention of Significant Deterioration (PSD). New source review for major sources in nonattainment areas is governed by Part D, Title I and Appendix S to 40 CFR Part 51.

Under both PSD and nonattainment NSR, the retrofit of a fume incinerator for control and reduction of VOC emissions to satisfy HON RCT requirements would be defined as a modification due to increased emissions of NOx and CO. Applicability to either regulation would depend upon the potential levels of these emissions from operation of the incineration unit. Secondary NOx and CO emissions resulting from installation of incineration to control process vent HON emissions for Model Plant Nos. 1, 2, and 3 (see Table 4) were evaluated as to their applicability under each regulatory program.

PSD --

A stationary source (i.e., chemical process plant) is defined as major if potential emissions of any pollutant for which that area is designated as attainment exceeds 100 tpy. If the facility evaluated as Model Plant Nos. 1, 2, or 3 was a major stationary source, the retrofit project must be evaluated to determine if it would be considered a major modification. As summarized in Table 4, the significant net emissions increase levels for NOx and CO under PSD are 40 and 100 tpy, respectively. From Table 4 it can be observed that Model Plant No. 1, 2, or 3 CO emissions would not trigger PSD review. Emissions of NOx from Model Plant Nos. 1 and 2 would not trigger PSD review; however, the retrofit project at Model Plant No. 3 would invoke PSD review as a major modification. The estimated NOx emission rate (161 Mg/yr, 177 tpy) exceeds the PSD de minimis rate of 40 tpy.

Model Plant No. 3 would also invoke PSD review if the facility were defined as a minor source before the project. The retrofit project at Model Plant

No. 3 (potential of 177 tpy of increased NOx emissions) would by itself be defined as a major source and subject to PSD review.

Among the requirements of PSD are:

- The facility must employ best available control technology (BACT) to control NOx from the project. [BACT is representative of the most stringent level of emission control with consideration given to economic, energy and environmental impacts.]
- Air quality impacts from the modification must be protective of PSD-defined air quality increments and the National Ambient Air Quality Standards.
- Secondary impacts due to the modification (e.g., impacts on soils, vegetation, visibility, demographics) must be assessed.
- Unless exempted, the facility must collect one year of ambient air quality monitoring data.

NONATTAINMENT NSR --

Title I of the 1990 CAA Amendments revised major stationary source and major modification definitions for ozone precursor (VOC and NOx) and CO emissions. If the facility (including all actively emitting operations) is considered a major stationary source for ozone (i.e., potential facility-wide VOC or NOx emissions greater than levels given in Table 9), when seeking a permit modification for the control equipment retrofit project, the facility will be forced to comply with major nonattainment NSR requirements if the project involves a significant increase in NOx emissions. If the facility is presently a minor source, the project itself would have to represent a major source of NOx to be subject to major nonattainment NSR. A similar analysis is applicable to potential CO emissions increases.

From Table 4 it can be observed that Model Plant No. 1, 2, or 3 CO emissions would not trigger nonattainment NSR. The maximum projected CO emissions increases from the three examples (26 Mg/yr, 29 tpy) are well below the lowest trigger level (i.e., 50 tpy for Serious CO nonattainment areas).

The model plant NOx emissions increases are affected differently depending upon the area (based upon ozone nonattainment classification, see Table 2) in which the plant is located. The modification represented by Model Plant No. 3 would trigger nonattainment NSR if located in any ozone nonattainment area regardless of location and classification. Model Plant No. 3 would also trigger

review if the facility was a minor source prior to the project because it alone represents a major stationary source. Model Plant Nos. 1 and 2 would only trigger nonattainment NSR as a modification in the Extreme ozone nonattainment area.

Among the requirements of the major nonattainment NSR program are:

- The facility must employ lowest achievable emission rates (LAER) to control NOx from the project. [LAER is representative of the most stringent level of emission control without regard for economical considerations.]
- The facility would be required to locate and secure NOx emission reductions (offsets) from any other facility operations or from nearby facilities at a ratio summarized in Table 9.
- The offsets secured by the facility must provide for a net air quality benefit.
- The owner/operator of the facility must demonstrate that all other major stationary sources owned by them within the State are subject to and in compliance with all applicable parts of the Clean Air Act.

2.4 NOx AND CO REGULATORY IMPACTS FOR MODEL PLANTS

The above sections provided a detailed discussion of regulatory issues for NOx and CO emissions from the thermal oxidizer systems. Tables 2 and 3 summarized the regulatory applicability for the process vent model plants. Based on Tables 2 and 3, Tables 10 and 11 summarize the regulatory applicability for the existing minor source and major source, respectively. For each model plant, the attainment and nonattainment permitting issues are indicated for CO and NOx.

SECTION 3 IMPACT EVALUATION FOR HALOGENATED STREAMS

Section 2 evaluation consisted of identification of multimedia impacts associated with the RCTs for three HON source categories (process vents, transfer and loading operations, and wastewater collection and treatment operations). This section evaluates the multimedia impacts associated with halogenated exhaust streams.

Treatment of halogenated gas streams via thermal oxidation generates gaseous hydrogen chloride. A combination thermal oxidizer/scrubber system will be required to control the halogenated exhaust streams. Operation of the scrubber will generate a wastewater stream that will require treatment and disposal. The scrubber will also require electrical energy for the pumps and pressure drop in the system. Table 12 presents the water rate data for the scrubber system for the process vent model plants. The rates are based on a liquid-to-gas ratio (gallons/1,000 scf) of 20 and a make-up water rate of 10 percent.

The operation of the scrubber will generate a low pH wastewater discharge that will require treatment and disposal. However, the disposal needs will depend upon the characteristics of the other wastewater streams present at the facility where model plant streams are present and treatment methods practiced at the facility.

SECTION 4 COST-EFFECTIVENESS OF NOx CONTROL

As outlined in Section 2, NOx emissions generated by thermal oxidizer systems proposed as MACT must be controlled to comply with the CAA regulations. The costs of controlling NOx generated by the thermal oxidizer systems for the CMA process vent model plants have been estimated to determine the NOx control cost-effectiveness.

The NOx present in the exhaust stream from the thermal oxidizer system is generated as "thermal NOx", i.e., nitrogen and oxygen present in the combustion air react to produce NOx. The NOx reduction approaches for thermal oxidizer systems consist of burner and combustion process modification. Post-combustion or add-on NOx control systems such as selective catalytic reduction or selective noncatalytic reduction are not practical for exhaust streams from thermal oxidizer systems because of the system complexity and costs. The applicability of the post-combustion NOx control methods is also questionable for the thermal oxidizer exhaust stream because of the relatively low NOx concentration level.

Low-NOx burner design is a primary method of NOx reduction available for the thermal oxidizer systems. This approach can also be combined with other measures such as exhaust gas recirculation and/or staged combustion. The specific modification employed will depend on the characteristics of the VOC-laden stream that is being controlled.

Table 13 presents the cost-effectiveness of the NOx control measures for the thermal oxidizer systems for the process vent model plants. The cost evaluation is based on the assumption that the NOx from thermal oxidizer system will be reduced by about 66 percent (from uncontrolled level of 150 ppm to 50 ppm) using a combination of low-NOx burner design and combustion modification measures. Based on EQ's experience, it is estimated that the NOx reduction measures will increase the capital cost of the equipment by about 20 percent. Using this assumption cost-effectiveness values for the process vent model plants are presented in Table 13.

Table 13 assumes that a single thermal oxidizer unit will be installed to handle the exhaust flow from each model plant. Although this assumption may be appropriate for the smaller model plants (1 and 2), larger model plants may require multiple systems for process control reasons. The cost-effectiveness of NOx control ranges from \$1,300 to \$22,300/Mg-yr of NOx controlled. Again, the costs of Model Plants 3 and 4 would be significantly higher since they will require installation of multiple thermal oxidizer units. NOx cost-effectiveness values of \$8,000/Mg-yr or higher are more realistic for the larger plants. The HAP cost-effectiveness values for the model plants are also shown in Table 13. The HAP cost-effectiveness values are significantly lower than the NOx cost effectiveness values.

SECTION 5 CONCLUSIONS

The analysis performed in this memo leads to following conclusions:

- Control of process vent source category model plants as defined by CMA results in significant quantities of NOx, CO, and SO₂ emissions.
- The electrical energy requirements for the CMA process vent model plants 3 and 4 are significant and result in significant SO₂ emissions.
- The NOx and CO emission rates for the loading rack and wastewater treatment sources are relatively minor.
- The HAP cost-effectiveness values are significantly lower than the NOx cost effectiveness values.

TABLE 1. STATES COMPRISING 90 PERCENT OF THE SOCMI CAPACITY

	Number of	Percent of
State	process units	national total
Texas	251	34
Louisiana	115	16
New Jersey	56	8
West Virginia	33	5
Illinois	26	4
North Carolina	20	3
Tennessee	18	2
Kentucky	17	2
Michigan	17	2
Pennsylvania	16	2
Alabama ·	15	. 2
California	15	2
Kansas	14	2
Ohio	14	2
New York	13	2
Indiana	9	1
South Carglina	8	1
	657	90
National Total	729	100

	Carbon Monoxide	<u> </u>	Nitrogen Dioxide	Ozone	· · · · · · · · · · · · · · · · · · ·
State	Area	Class	Area	Area	Class
					1
Texas	Portion of the City of El Paso (El Paso County)	Moderate ≤ 12.7 ppm	(none)	Beaumont-Port Arthur area	
				Hardin County	Serious ·
				Jefferson County	Serious
				Orange County	Serious
				Dallas-Fort Woth area	İ
	i			Collin County	Moderate
				Dallas County	Moderate
	4 .			Denton County	Moderate
				Tarrant County	Moderate
	· ·			El Paso County	Serious
		'		Houston-Galveston-Brazoria area	
				Brazoria County	Severe-17
				Chambers County	Severe-17
		ł I		Fort Bend County	Severe-17
				Galveston County	Severe-17
				Harris County	Severe-17
•				Liberty County	Severe-17
	•	Ļ		Montgomery County	Severe-17
				Waller County	Severe-17
				Victoria County	(Incomplete)
				<u>l</u>	1
Louisiana	(none)		(none)	Baton Rouge Area	
		[Ascension Parish	Serious
]		East Baton Rouge Parish	Serious
				Iberville Parish	Serious
	<u> </u>			Livingston Parish	Serious
	· .			Pointe Coupee Parish	Serious
				West Baton Rouge Parish	Serious
			•	Beauregard Parish	(Incomplete)
				Grant Parish	(Incomplete)
		<u>'</u>		Lafayette Parish	Transitional
				Lafourche Parish	(Incomplete)
				Calcasieu Parish	Marginal
	j.		l	New Orleans area	
				Jefferson Parish	Transitional
		ļ		Orleans Parish	Transitional
	i		İ	St. Bernard Parish	Transitional
				St. Charles Parish	Transitional
	1		1	St. James Parish	(incomplete)
				St. Mary Parish	(Incomplete)
]		
New Jersey	City of Atlantic City (Atlantic County)	Not Classified	(none)	Warren County	Marginal
-	City of Burlington (Burlington County)	Not Classified		Atlantic County	Moderate
	Borough of Freehold (Monmouth County)	Not Classified	1	Cape May County	Moderate
	City of Morristown (Morristown County)	Not Classified	l	New York-N. New Jersey-Long Island area	
	Bergen, Essex, Hudson, Union Counties	Moderate > 12.7 ppm	ĺ	Bergen County	Severe-17
	Cities of Clifton, Patterson, Passaic (Passaic County)	Moderate > 12.7 ppm		Essex County	Severe-17
	Portion of the Borough of Penns Grove (Salem County)	Not Classified	ĺ	Hudson County	Severe-17
	City of Perth Amboy (Middlesex County)	Not Classified		Hunterdon County	Severe-17
	ICITA DI LELLI VILIDOA MANDRIESEN CORTILA)				
			1	Middlesex County	Severe-17
	Camden County	Moderate ≤ 12.7 ppm		Middlesex County Monmouth County	Severe-17 Severe-17
				Middlesex County Monmouth County Morris County	

Carbon Mon				Ozone	
State	Area	Class	Area	Area	Class
		,			
				Passaic County	Severe-17
				Sommerset County	Severe-17
				Sussex County	Severe-17
				Union County	Severe-17
				Philadelphia-Wilmington-Trenton Area	
				Burlington County	Severe-15
				Camden County	Severe-15
					Severe-15
				Cumberland County	
				Gloucester County	Severe-15
				Mercer County	Severe-I
	A STATE OF THE PARTY OF THE PAR			Salem County	Severe-15
West Virginia	(none)		(none)	Kanawha County	Moderate
A STATE OF THE PARTY OF	Junior		Auctiva	Putnam County	Moderate
					Marginal
		The second secon		Greenbrier County	
				Cabell County	Moderate
				Wayne County	Moderate
				Wood County	Moderati
Illinois	(none)		(none)	Chicago-Gary-Lake County Area:	
				Cook County	Severe-1
				Du Page County	Severe-17
				Aux Sable, Gooselake Townships (Grundy County)	
				Kane County	Severe-17
				Oswego Township (Kendall County)	Severe-17
				Lake County	Severe-1
		The second second		McHenry County	Severe-1
				Will County	Severe-1
				Jersey County	Margina
				St. Louis Area:	Trial B.
				Madison County	Moderat
				Monroe County	Moderat
				St. Clair County	Moderat
North Carolina	Mecklenburg County	Not Classified	(none)	Gaston County	Moderat
	Durham County	Moderate ≤ 12.7 ppm		Mecklenburg County	Moderat
	Wake County	Moderate ≤ 12.7 ppm		Davidson County	Moderat
	Forsyth County	Moderate ≤ 12.7 ppm		Portion of Davie County	Moderat
		A CONTRACT TO SECOND		Forsyth County	Moderat
				Guilford County	Moderat
		The state of the s		Durham County	Moderat
				Dutchville Township (Granville County)	Moderat
				Wake County	Moderat
Tennessee	Shelby County	Moderate ≤ 12.7 ppm	(none)	Knox County	Margina
				Shelby County	Margina
	The second secon			Nashville Area:	
				Davidson County	Moderat
	The second secon			Rutherford County	Modera
					The state of the s
				Sumner County	Moderat
				Williamson County	Moderat
				Wilson County	Moderat

*	Carbon Monoxide	Nitrogen Dioxide	Ozone		
State	Area	Class	Area	Area	Class
	, ,				
Kentucky	(none)		(none)	Cincinnati Area:	
	•			Boone County	Moderate
				Campbell County	Moderate
			i e	Kenton County	Moderate
			l	Edmonson County	Rural Transpor
			ļ	Huntington-Ashland Area:	į
				Boyd County	Moderate
		•	1	Portion of Greenup County	Moderate
				Lexington Area:	
				Fayette County	Marginal
		•		Scott County	Marginal
		}	ł	Louisville Area:	i was garan
		Į		L	
		l l	i	Portion of Bullitt County	Moderate
		Į.		Jefferson County	Moderate
		(i	Portion of Oldham County	Moderate
	,	1	i	Owensboro Area:	1
	.	i i		Daviess County	Marginal
		1		Portion of Hancock County	Marginal
	ļ		l	Portion of Livingston County	Marginal
		•		Marshall County	Marginal
Michigan	Detroit Area:		(none)	Allegan County	(Incomplete)
MICHIBAN	Portions of the City of Detroit	Not Classified	(none)	Barry County	(Incomplete)
			1	Calhoun County	(Incomplete)
	Portions of Macomb, Oakland, Wayne Counties	Not Classified	1		
		1	1	Berrien County	(Incomplete)
				Branch County	(incomplete)
	· · ·	1	Ì	Cass County	(Incomplete)
			ł	Detroit-Ann Arbor Area:	
			1	Livingston County	Moderate
	1	1		Macomb County	Moderate
			ļ.	Monroe County	Moderate
		1		Oakland County	Moderate
		1	j	St. Clair County	Moderate
		1	ĺ	Washtenaw County	Moderate
		1		Wayne County	. Moderate
		1		Genesee County	Transitional
	1	1		Grand Rapids Area:	
			1	Kent County	Moderate
			1		Moderate
		1		Ottawa County	B 1
		1 '		Gratiot County	(Incomplete)
			1	Hillsdale County	(Incomplete)
				Huron County	(Incomplete)
	ì	1		Ionia County	(Incomplete)
			†	Jackson County	(Incomplete)
				Kalamazoo County	(Incomplete)
	· ·			Lansing-East Lansing Area:	i ·
		1	1	Clinton County	Transitional
	{		i	Eaton County	Transitional
		i			Transitional
	İ	j		Ingham County	
		1	,	Lapeer County	(Incomplete)
	ł	1		Lenatvee County	(Incomplete)
	1	1		Montcalm County	(Incomplete)
	1	ľ	1	Muskegon County	Serious

	Carbon Monoxide		Nitrogen Dioxide	Ozone	
State	Area	Class	Area	Area	Class
				Bay County	(Incomplet
				Midland County	(Incomplet
				Saginaw County	(Incomplet
				Sanflac County .	(Incomplet
				Shiawassee County	(Incomplet
				St. Joseph County	(Incomplet
				Tuscola County	(Incomplet
				Van Buren County	(Incomplet
ennsylvania	Portions of the City of Phildelphia (Phil. County)	Moderate ≤ 12.7 ppm	(none)	Allentown-Bethlehem-Easton Area:	7
	Portions of the City of Pittsburgh (Allegheny County)	Not Classified		Carbon County	Margina
				Lehigh County	Margina
				Northhampton County	Margina
				Blair County	Margina
				Crawford County	(Incomple
				Erle County	Margina
				Franklin County	(Incomple
					(Incomple
				Greene County	furnithis
				Harrisburg-Lebanon-Carlisle Area:	Manufacture
				Cumberland County	Margina
				Dauphin County	Margina
				Lebanon County	Margin
	The second secon			Perry County	Margina
				Johnstown Area:	
				Cambria County	Margina
				Somerset County	Margina
				Juniata County	(Incomple
				Lancaster County	Margina
				Lawrence County	(Incomple
				Northumberland	(Incomple
				Philadelphia-Wilmington-Trenton Area:	timeompie
	A STATE OF THE PARTY OF THE PAR				Severe-1
				Bucks County	Severe-1
				Chester County	COLUMN TO SERVICE OF THE PARTY
				Delaware County	Severe-
				Montgomery County	Severe-
	THE RESERVE OF THE PARTY OF THE			Philadelphia County	Severe-1
				Pike County	(Incomple
	the state of the s			Pittsburgh-Beaver Valley Area:	
	the same was the same of the s			Allegheny County	Modera
	The state of the s			Armstrong County	Modera
	the state of the s			Beaver County	Modera
				Butler County	Modera
				Favette County	Moderal
					Modera
				Washington County	
	The second secon			Westmoreland County	Modera
	No. of the second second			Berks County	Modera
				Schuykill County	(Incomple
	The state of the s			Scranton-Wilkes Barre Area:	
				Columbia County	Margin
				Lackawanna County	Margin
				Luzerne County	Margin
	the state of the s			Monroe County	Margin
				Wyoming County	Margin

	Carbon Monoxide		Nitrogen Dioxide	Ozone	
State	Area	Class	Area	Area	Class
					1 " , , ,
			Ì	Susquehanna County	(Incomplete)
	•			Warren County	(Incomplete)
				Wayne County	(Incomplete)
				York Area:	
				Adams County	Marginal
			j	York County	Marginal
	·			Mercer County	Marginal
Alabama	(none)		(none)	Birmingham Area:	l
				Jefferson County	Marginal
				Shelby County	Marginal
		:		Cherry County	
California	Bakersfield Area:		South Coast Air Basin	Butte County	Transitional
	Portion of urban Bakersfield (Kern County)	Not Classified	ľ	Imperial County	Transitional
	Portion urban Chico (Butte County)	Moderate ≤ 12.7 ppm	4	Los Angeles-South Coast Air Basin (LA County)	Extreme
	Portion of urban Fresno (Fresno County)	Moderate ≤ 12.7 ppm	1	Orange County	Extreme
	Portion of Placer County (Lake Tahce North Shore)	Not Classified		Portions of Riverside County	Extreme
		Moderate ≤ 12.7 ppm	1	Portions of San Bernadino County	Extreme
	Portions of the City of Los Angeles (Los Angeles County			Monterey Bay Area:	
	Orange County	Serious		Monterey Bay	Moderate
	Portions of Riverside County	Serious		San Benito County	Moderate
		Serious	1		Moderate
	Portions of San Bernadino County	Serious	Í	Santa Cruz County	Moderate
	Modesto Area:	l		Sacramento Area:	C
	Portion of urban Modesto (Stanislaus County)	Moderate ≤ 12.7 ppm	l .	Portions of El Dorado County	Serious
	Sacramento Area:	1		Portions of Placer County	Serious
	Portion of urban Placer County	Moderate ≤ 12.7 ppm		Sacramento County	Serious
	Portion of urban Sacramento County	Moderate ≤ 12.7 ppm	1	Portions of Solano County	Serious
•	Portion of urban Yolo County	Moderate ≤ 12.7 ppm	i <u>l</u>	Portions of Sutter County	Serious
	Portions of San Diego County	Moderate ≤ 12.7 ppm	i e	Yolo County	Serious
	San Francisco-Oakland-San Jose Area:	1		San Diego County	Severe-15
	Portion of urban Alameda County	Moderate ≤ 12.7 ppm	1	San Francisco-Bay Area:	
	Portion of urban Contra Costa County	Moderate ≤ 12.7 ppm		Alameda County	Moderate
	Portion of urban MArin County	Moderate ≤ 12.7 ppm		Contra Costa County	Moderate
	Portion of urban Napa County	Moderate ≤ 12.7 ppm		Marin County	Moderate
	Portion of urban San Francisco County	Moderate ≤ 12.7 ppm		Napa County	Moderate
				San Francisco County	Moderate
	Portion of urban San Mateo County	Moderate ≤ 12.7 ppm Moderate ≤ 12.7 ppm		San Mateo County	Moderate
	Portion of urban Santa Clara County			•	Moderate
	Portion of urban Solano County	Moderate ≤ 12.7 ppm		Santa Clara County	Moderate
	Portion of urban Sonoma County	Moderate ≤ 12.7 ppm		Portions of Solano County	Moderate
	Portion of urban Stockton (San Joaquin County)	Moderate ≤ 12.7 ppm	1	Portions of Sonoma County	Moderate
			1	San Joaquin Valley Area:	1 .
				Fresno County	Serious
			ŀ	Kern County	Serious
	İ	ŀ	1	Kings County	Şerious
			1	Madera County	Serious
		1	1	Merced Coujty	Serious
				San Joaquin County	Serious
		1	1	Stanilaus County	Serious
	<u> </u>		1 .	Tulare County	Serious
		1		Santa Babara County	Moderate
			}	Southeast Desert Modified Area:	acrine
		j	ľ	Postions of Les Appeles County	Severe-17
		1	1	Portions of Los Angeles County	1
	1	1		Portions of Rivberside County	Severe-17
	· 1	1	1	Portions of San Bernadino County	Severe-17

	Carbon Monoxide		Nitrogen Dioxide	Ozone	
State	Area	Class	Area	Area	Class
				Ventura County	Severe-15
				Yuba City Area:	-
	A STATE OF THE PARTY OF THE PAR			Portions of Sutter County	Transitional
				Yuba County	Transitional
Kansas	(none)		(none)	(none)	
Ohio	Cuyahoga County	Moderate ≤ 12.7 ppm	(none)	Stark County	Marginal
				Cincinnati-Hamilton Area:	
				Butler County	Moderate
				Clermont County	Moderate
				Hamilton County	Moderate
	The state of the s			Warren County	Moderate
				Cleveland-Akron-Lorain Area:	-
				Ashtabula County	Moderate
				Cuyahoga County	Moderate
				Geauga County	Moderate
				Lake County	Moderate
				Lorain County	Moderate
				Medina County	Moderate
	the second secon			Portage County	Moderate
	The same of the sa			Summit County	Moderate
				Clinton County	Transitional
				Columbiana County	(Incomplete)
				Columbus Area:	and the same
				Delaware County	Marginal
				Franklin County	Marginal
	and the second s	and the same of th		Licking County	Marginal
				Dayton-Springfield Area:	
		The state of the s		Clark County	Moderate
	The second secon			Greene County	Moderate
				Miami County	Moderate
				Montgomery County	Moderate
		The second second		Preble County	Transitional
				Jefferson County	Transitional
				Toledo Area:	Hansicichai
	The state of the s	The second second			Moderate
				Lucas County Wood County	Moderate
	the state of the s	100		Youngstown-Warren-Sharon Area:	Moderate
				Mahoning County	Marginal
					Marginal
		THE REAL PROPERTY.		Trumbull County	Margina
New York	New York-North New Jersey-Long Island Area:		(none)	Albany-Schenectady-Troy Area:	
	Bronx County	Moderate > 12.7 ppm		Albany County	Marginal
	Kings County	Moderate > 12.7 ppm		Greene County	Marginal
	Nassau County	Moderate > 12.7 ppm		Montgomery County	Marginal
	New York County	Moderate > 12.7 ppm		Rensselaer County	Marginal
	Queens County	Moderate > 12.7 ppm		Saratoga County	Marginal
	Richmond County	Moderate > 12.7 ppm		Schenectady County	Marginal
	Westchester County	Moderate > 12.7 ppm		Buffalo-Niagara Falls Area:	
	Onondaga County	Moderate ≤ 12.7 ppm		Erie County	Marginal
				Niagara County	Marginal
				Portons of Essex County	Rural Transpor
	The second secon			Jefferson County	

	Carbon Monoxide		Nitrogen Dioxide Area	Ozone		
State	Area	Class		Area	Class	
Indiana	Portions of the City of East Chicago (Lake County) Portions of the City of Indianapolis (Marion County)	Not Classified Not Classified	(none)	New York-North New Jersey-Long Island Area: Bronx County Kings County Nassau County New York County Orange County Putnam County Queens County Richmond County Sulfolk County Westchester County Dutchess County Chicago-Gary-Lake County Area: Lake County Porter County Vanderburgh County Marion County Louisville Area: Clark County Floyd County South Bend-Elkhart Area: Elkhart County St. Joseph County	Severe-17 Severe-17 Severe-17 Severe-17 Severe-17 Severe-17 Severe-17 Severe-17 Severe-17 Marginal Severe-17 Marginal Moderate Moderate Marginal Marginal	
South Carolina	(none)		(none)	Cherokee County	Marginal	

TABLE 3. MODEL PLANT PARAMETERS FOR THE HON SOURCE CATEGORIES

Source Category	Model Plant Parameters
1. Process venus	1. Stream flow rate = 100 scmm HAP = hexane HAP concentration = 299 ppmv
	2. Stream flow rate = 1000 scmm HAP = hexane HAP concentration = 116 ppmv
	3. Stream flow rate = 10,000 scmm HAP = hexane HAP concentration = 98 ppmv
	4. Stream flow rate = 100,000 scmm HAP = hexane HAP concentration = 96 ppmv
2. Transfer and loading operations	20 model plants defined in the BID
3. Wastewater collection and treatment operations	18 model plants defined in the BID

TABLE 4. SECONDARY IMPACTS FOR INCINERATION CONTROL OF CMA MODEL PROCESS VENT STREAMS

Model			H/	AP Emissions		Second	dary NOX	Second	lary CO
Plant No.	Source Description	Control Device	Uncontrolled, Mg/yr	Controlled, Mg/yr	Reduction, Mg/yr	Emissions, Mg/yr	NOX-to-HAP Ratio	Emissions, Mg/yr	CO-to-HAP Ratio
1	100 scmm flow with 299 ppmv hexane as only VOC	Thermal Incineration	51.75	1.04	51	1.48	0.029	0.260	0.005
2	1,000 scmm flow with 116 ppmv hexane as only VOC	Thermal Incineration	202	4.04	198	16.0	0.081	2.34	0.012
3	10,000 scmm flow with 98 ppmv hexane as only VOC	Thermal Incineration	1,697	33.9	1,663	161	0.097	26.0	0.016
4	100,000 scmm flow with 96 ppmv hexane as only VOC	Thermal Incineration	16,625	333	16,293	1610	0.099	260	0.016

TABLE 5. SECONDARY IMPACTS FOR INCINERATION CONTROL OF EPA MODEL PROCESS VENT STREAMS

Model			HA	AP Emissions		Second	dary NOX	Second	dary CO
Plant	Source	Control	Uncontrolled,	Controlled,	Reduction,	Emissions,	NOX-to-HAP	Emissions,	CO-to-HAP
No.	Description	Device	Mg/yr	Mg/yr	Mg/yr	Mg/yr	Ratio	Mg/yr	Ratio
1	Formaldehyde via Air Oxidation	Thermal Incineration	91.6 (a)	12.2	79 (a)	0.0316	0.0004 (a)	0.00394	0.00005 (a)
2	Air Oxidation	Thermal Incineration	2770	55.4	2715	355	0.131	23.4	0.0086
3	Phthalic Anhydride via Air Oxidation	Thermal Incineration	876 (a)	117	759 (a)	3.66	0.0048 (a)	0.455	0.0006 (a)
4	Perephthalic Acid via Air Oxidation	Thermal Incineration	6100	122	5978	624.9	0.105	18.8	0.0031
5	Distillation NV	Incinerator and Scrubber	8.46 (a)	1.69	6.8 (a)	0.000201	0.00003 (a)	0.0000249	0.000004 (a)
6	Distillation V	Thermal Incineration	6.36	0.127	6.23	0.186	0.030	0.0148	0.0024
7	Ethylbenzene	Flare	3.38	0.0676	3.31	0.0141	0.0043	0.0171	0.0052
8	Formaldehyde	Flare	0.139	0.00279	0.13621	0.0168	0.123	0.00675	0.0496
9	Adiponitrile via Hydrodimerization.	Thermal Incineration	92.2	1.84	90.4	5.26	0.058	0.408	0.0045
10	Ethylene Glycol Monoethyl Ether Acetate via Esterification	Flare	13.6	0.273	13.3	0.0153	0.0011	0.00632	0.0005
11	Halogenation	Incinerator and Scrubber	15	0.3	14.7	1.13	0.077	0.055	0.0037
12	Condensation	Flare	0.337	0.00675	0.330	0.0141	0.043	0.0059	0.0179

⁽a) These numbers are suspect. The uncontrolled HAP generation values were not calculated following the same calculation procedures as the other model plants emissions. Typographical errors suspected.

TABLE 6. ELECTRICAL ENERGY REQUIREMENTS AND SO₂ EMISSION RATES FOR THE PROCESS VENT MODEL PLANTS

Flow rate, scmm	Electricity rating, kW	Annual energy requirement, kWh/yr	Coal consumption, tpy	SO ₂ emission rate, tpy
100	14	121,000	50	1
1,000	138	1,213,000	505	7
10,000	1,384	12,127,000	5,053	73
100,000	13,843	121,268,000	50,528	<i>7</i> 28

Model			H/	AP Emissions		Second	ary NOX	Second	dary CO
Rack	Model	Control	Uncontrolled,	Controlled,	Reduction,	Emissions,	NOX-to-HAP	Emissions,	CO-to-HAP
No.	Description	Device	Mg/yr	Mg/yr	Mg/yr	Mg/yr	Ratio	Mg/yr	Ratio
	Tank car rack with 3 arms handling 1 chemical; Max. through 0.00831 MMgal/yr; Avg. v.p. 0.210 mmHG	Flare	3.63E-06	7.30E-08	3.56E-06	2.25E-05	6.33E+00	9.01E-06	2.53E+00
	MOYOUGD D DE'45 MANGONYE	Thermal incinerator/ scrubber	6.44E-04	1.29E-05	6.31E-04	3.62E-05	5.74E-02	7.37E-06	1.17E-02
3	Tank car rack with 3 arms handling 1 chemical; Max. through 0.300 MMgal/yr; Avg. v.p. 0.250 mmHG	Flare	1.45E-04	2.89E-06	1.42E-04	8.00E-05	5.63€-01	3.20 ∈ -05	2.25E-01
4	Tank car rack with 3 arms handling 4 chemicals; Max. through 4.65 MMgal/yr; Avg. v.p. 149 mmHG	Thermal incinerator/ scrubber	3.14E-02	6.29E-04	3.08E-02	1.05E-02	3.41E-01	4.23E-04	1.37E-02
5	Tank car rack with 3 arms handling 1 chemical; Max. through 1.23 MMgal/yr; Avg. v.p. 6.59 mmHG	Flare	9.38E-02	1.88E-03	9.19E-02	2.91E-03	3.17E-02	1.16E-03	1.26E-02
6 .	Tank car rack with 16 arms handling 4 chemicals; Max. through 33.3 MMgal/yr; Avg. v.p. 889 mmHG	Thermal incinerator/scrubber	3.46E+00	6.91E-02	3.39E+00	1.88E-02	5.54E-03	3.60E-03	1.06E-03
7	Tank car rack with 8 arms handling 1 chemical; Max. through 12.9 MMgal/yr; Avg. v.p. 6.59 mmHG	Flare	9.83E-01	1.96E-02	9.63E-01	2.98E-02	3.09E-02	1.19E-02	1.24E-02

Model			H/	AP Emissions		Second	dary NOX	Secondary CO	
Rack	Model	Control	Uncontrolled,	Controlled,	Reduction,	Emissions,	NOX-to-HAP	Emissions,	CO-to-HAP
No.	Description	Device	Mg/yr	Mg/yr	Mg/yr	Mg/yr	Ratio	Mg/yr	Ratio
8	Tank car rack with 8 arms handling 2 chemicals; Max. through 16.5 MMgal/yr; Avg. v.p. 8.42 mmHG	Flare	1.71E+00	3.42E-02	1.68E+00	3.96E-02	2.36E-02	1.58E-02	9.43E-03
9	Tank car rack with 16 arms handling 4 chemicals; Max. through 45.6 MMgal/yr; Avg. v.p. 15.2 mmHG	Thermal incinerator	6.52E+00	1.30E-01	6.39E+00	1.26Ë-01	1.97E-02	2.53E-03	3.96E-04
10	Tank car rack with 10 arms handling 5 chemicals; Max. through 22.2 MMgal/yr; Avg. v.p. 327 mmHG	Thermal incinerator	5.76E+00	1.15E-01	5.65E+00	1.21E-02	2.14E-03	1.14E-03	2.02E-04
11	Tank truck rack with 1 arm handling 1 chemical; Max. through 0.00548 MMgal/yr; Avg. v.p. 0.210 mmHG	Flare	2.39E-06	4.80E-08	2.34E-06	1.60E-05	6.83E+00	6.41E-06	2.74E+00
12	Tank truck rack with 3 arms handling 1 chemical; Max. through 0.0635 MMgal/yr; Avg. v.p. 1.00 mmHG	Thermal incinerator/scrubber	6.44E-04	1.29E-05	6.31E-04	3.62E-05	5.74E-02	7.38E-06	1.17E-02
13	Tank truck rack with 1 arm handling 2 chemicals; Max. through 2.27 MMgal/yr; Avg. v.p. 703 mmHG	Flare	3.02E-04	6.04E-06	2.96E-04	5.43E-03	1.83E+01	2.17E-03	7.33E+00
14	Tank truck rack with 2 arms handling 2 chemicals; Max. through 5.68 MMgal/yr; Avg. v.p. 566 mmHG	Flare	9.92E-04	1.98E-05	9.72E-04	1.26E-02	1.30E+01	5.03E-03	5.17E+00
15	Tank truck rack with 1 arm handling 9 chemicals; Max. through 0.756 MMgal/yr; Avg. v.p. 11.9 mmHG	Thermal incinerator/scrubber	2.12E-01	4.25E-03	2.08E-01	4.01E-03	1.93E-02	1.26E-04	6.06E-04

Model			H/	AP Emissions		Second	lary NOX	Second	lary CO
Rack	Model	Control	Uncontrolled,	Controlled,	Reduction,	Emissions,	NOX-to-HAP	Emissions,	CO-to-HAP
No.	Description	Device	Mg/yr	Mg/yr	Mg/yr	Mg/yr	Ratio	Mg/yr	Ratio
16	Tank truck rack with 4 arms handling 10 chemicals; Max. through 7.84 MMgal/yr; Avg. v.p. 592 mmHG	Flare	2.15E-01	4.30E-03	2.11E-01	1.72E-02	8.16E-02	6.88E-03	3.27E-02
	Fank truck rack with 2 arms handling 11 chemicals; Max. through 4.40 MMgal/yr; Avg. v.p. 659 mmHG	Flare	8.72E-01	1.74E-02	8.55E-01	9.73E-03	1.14E-02	3.89E-03	4.55E-03
18	narawan is x mmazivr ava i	Thermal incinerator/ scrubber	4.55E+00	9.11E-02	4.46E+00	1.10E-02	2.47E-03	1.80E-03	4.04E-04
19	Tank truck rack with 2 arms handling 2 chemicals; Max. through 3.70 MMgal/yr; Avg. v.p. 128 mmHG	Thermal incinerator/ scrubber	4.30E+00	8.61E-02	4.21E+00	3.80E-03	9.02E-04	5.40E-04	1.28E-04
	Tank truck rack with 4 arms handling 4 chemicals; Max. through 30.2 MMgal/yr; Avg. v.p. 131 mmHG	Flare	1.97E+01	3.95E-01	1.93E+01	6.36E-02	3.29E-03	2.54E-02	1.32E-03

TABLE 8. SECONDARY IMPACTS FOR STREAM STRIPPER CONTROL OF EPA MODEL WASTEWATER STREAMS

Model	Mod	del Descript	ion	HAP Em	issions	Second	dary PM	Second	lary SO2	Second	dary NOX	Second	dary CO
Stream	Flow,	HAP Conc.		Uncontrolled,	Reduction,	Emissions,	PM-to-HAP	Emissions,	SO2-to-HAP	Emissions,	NOX-to-HAP	Emissions,	CO-to-HAP
No.	lpm/Gg/yr	mg/l	Volatility	Mg/yr	Mg/yr	Mg/yr	Ratio	Mg/yr	Ratio	Mg/yr	Ratio	Mg/yr	Ratio
4	0.05	10	low	0.0016	0.003	0.006	2.0	0.05	16.7	0.15	50	0.02	6.67
5	0.05	250	low	0.039	0.0073	0.006	0.82	0.05	6.85	0.15	20.5	0.02	2.74
6	0.05	5000	low ·	0.79	0.15	0.006	0.04	0.05	0.33	0.15	. 1	0.02	0.13
46	0.05	10	medium- high	0.013	0.034	0.006	0.18	0.05	1.47	0.15	4.41	0.02	0.59
47	0.05	250	medium- high	0.33	Q. 8 5	0.006	0.007	0.05	0.06	0.15	0.18	0.02	0.02
48	0.05	5000	medium- high	6.6	16.9	0.006	0.0004	0.05	0.003	0.15	0.009	0.02	0.001
67	0.05	10	high	0.036	0.13	0.006	0.046	0.05	0.38	0.15	1.15	0.02	0.15
68	0.05	250	high	0.89	3.2	0.006	0.002	0.05	0.02	0.15	0.05	0.02	. 0.006
69	0.05	5000 ·	high	17.9	64.4	0.006	0.00009	0.05	0.0008	0.15	0.002	0.02	0.0003
19	250	10	low	0.016	0.0029	0.06	20.7	0.5	172	. 1.5	517 ·	0.2	69.0
20	250	200	low	0.32	0.058	0.06	1.03	0.5	8.62	1.5	25.9	0.2	3.45
21	250	1600	low	2.5	0.46	0.06	0.13	0.5	1.09	1.5	3.26	0.2	0.43
61	250	10	medium- high	0.13	0.34	0.06	0.18	0.5	1.47	1.5	4.41	0.2	0.59
62	250	200	medium- high	2.6	6.8	0.06	0.009	-0.5	0.07	1.5	0.22	0.2	0.03
63	250	1600	medium- high	21	54.2	0.06	0.001	0,5 ·	0.009	1.5	0.03	0.2	0.004
82	250	·10	high	0.36	1.3	0.06	0.046	0.5	0.38	1.5	1.15	0.2	0.15
83	250	200	high	7.1	25.8	0.06	0.002	0.5	0.02	1.5	0.06	0.2	0.008
84	250	1600	high	57.2	206.1	0.06	0.0003	0.5	0.002	1.5	0.007	0.2	0.0010

TABLE 9. SUMMARY OF MAJOR NEW SOURCE REVIEW APPLICABILITY CITERIA

	Potentiallemission rate				
	defining major sources in	Net emissions incr		Normal NNSF	
Criteria Pollutant/	nonattainment areas,	defining a major modific	ation (2)	Emission	
Area Designation	tpy	PSI), tpy	NNSR, φy	Offset Ratio	
Carbon Monoxide					
Unclassifiable/Attainment	See Note (1)	100			
Nonattainment:					
Not Classified	100		100	1.1:1	
Marginal ≤ 12.7 ppm	100	•	100	1.1:1	
Marginal > 12.7 ppm	100		100	1.1:1	
Serious	50		50	1.1:1	
Nitrogen dioxide					
Unclassifiable/Attainment	See Note (1)	40			
Nonartainment	100		40	1.1:1	
Ozone (as VOC or NOx)					
Unclassifiable/Attainment	See Note (1)	40 (VOC only)			
Nonattainment:					
Marginal (3)	100		` 40/40	1.1:1	
Moderate	100		40/40	1.15:1	
Serious	50		25/25	1.2:1	
Severe (4)	25		25/25	1.3:1	
Extreme	10		Any ner increase	1.5:1	

NOTES:

- (1) Stationary sources located in attainment areas are defined as major if potential emissions of any pollutant for which an area is attainment are greater than 100 tpy for 28 listed categories (including chemical process plants) or 250 tpy for all other source categories.
- (2) PSI) Prevention of Significant Detenioration (\$52.21)

 NNSR Nonattainment new source review (40 OFR Part 51, Appendix S)
- (3) Includes areas designated as Transitional and Rural Transport, and those with Incomplete Data.
- (4) Includes Severe-15 and Severe-17 areas.

TABLE 10. SUMMARY OF REGULATORY APPLICABILITY FOR EXISTING MINOR SOURCE

		NOX	8	Attainn	nent Areas		No	nattainment A	reas (Emissio	on Offset Poli	Offset Policy)				
Model		emissions,	emissions,	(PS	D)	С	0			Ozone (NOX)	one (NOX)				
Plant	Source Description	Mg/yr (tpy)	Mg/yr (tpy)	NOX	ω	Moderate	Serious	Marginal	Moderate	Serious	Severe	Extreme			
1	100 scmm air flow, 299 ppmv VOC (hexane)	1.5 (1.7)	0.3 (0.33)												
2	1,000 scmm air flow, 116 ppmv VOC (hexane)	16 (18)	2.3 (2.6)		:							4			
3	10,000 scmm air flow, 98 ppmv VOC (hexane)	161 (178)	26 (29)	4				4	4	4	4	4			
4	100,000 scmm air flow, 96 ppmv VOC (hexane)	1610 (1780)	260 (290)	1	1	4	4	1	1	4	1	4			

(1) - indicates applicability of regulations to source modification

TABLE 12. SCRUBBER WATER RATES

	-		Water		rate	
Model Plant	Size, semm	Sign schm	circulation rate,	Gallons per minute	Million gallons/day	Million gallons/yr
1 .	100	3,531	71	7	0.01	4
2	1,000	\$5,315	706	71	0.10	37
3	10,000	353,147	7,063	706	1.02	371
4	100;000	3,531,467	70,629	7,063	10.17	3,712

TABLE 13. NOx CONTROL COST-EFFECTIVENESS FOR THERMAL OXIDIZER SYSTEMS

		Ba	seline Thermal	Oxidizer Syste	m .		Thermal Oxi	dizer System w	vith Low NOx	Costs Associated with NOx Control			
Model Plant	Size, scmm	Capital Cost, \$	Operating Cost, \$/yr	Capital Charge, \$/yr	Total Annualized Cost, \$/yr	HAP cost- effectiveness, \$/Mg-yr	Capital Cost, \$	Operating Cost, \$/yr	Capital Charge, \$/yr	Total Annualized Cost, \$/yr	Incremental Annualized Cost, \$/yr	NOx Controlled, Mg/yr	NOx Cost- effectiveness, \$/Mg/yr
1	100	428,000	25,000	107,000	132,000	2,603	514,000	25,000	129000	154,000	22,000	1	22,300
2	1,000	1,706,000	247,000	427,000	674,000	3,405	2,047,000	247,000	512000	759,000	85,000	11	8,000
3	10,000	6,790,000	2,472,000	1,698,000	4,170,000	2,507	8,148,000	2,472,000	2037000	4,509,000	339,000	107	3,200
4	100,000	27,031,000	24,720,000	6,758,000	31,478,000	1,932	32,437,000	24,720,000	8109000	32,829,000	1,351,000	1073	1,300
	<u> </u>								<u> </u>	<u> </u>	<u> </u>	<u> </u>	

APPENDIX D

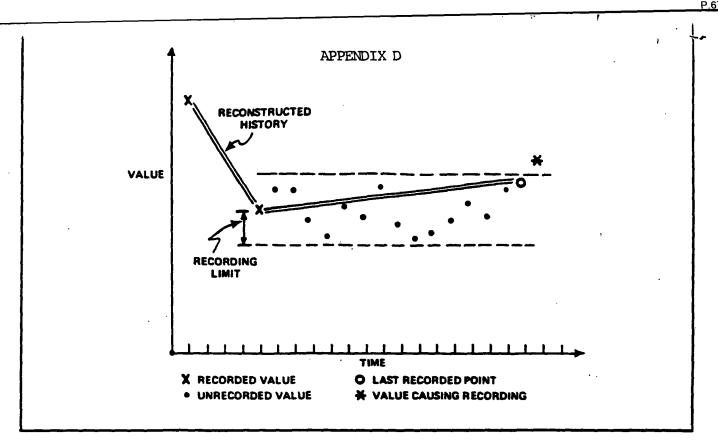


Figure 1. Box car algorithm.

Putting Computers to Work:

Historical Data Recording For Process Computers

Although process historians have demonstrated their benefits, it's often hard to convince people of how adaptable they are. Handson experience usually does the trick.

John C. Hale, E. I. Du Pont De Nemours, Wilmington, Del. 19898, Harold L. Sellars, Southwest Texas State Univ., San Marcos, Texas 78666

Computers have been used to monitor and control chemical and refining processes for more than 15 years. During this time, there has been a steady growth in the variety and sophistication of the functions performed by these process computers. Early systems were limited to maintaining only current operating measurements, available through crude operator's consoles or noisy teletypes. The value of retaining a process history, that is, a collection of measurements over time, became apparent, and early efforts produced shift and daily summary reports. The need for improved

process historians which record, retrieve and display process information has grown as process computers assume larger responsibilities in plant operations.

Du Pont has developed process historian functions that have been used on several of its in-house process monitoring and control systems (1). This work has evolved to meet both the increasing computer capability and the demand for better availability of process information for operators and engineers. Data compression techniques have been applied to permit ever increasing data storage to remain accessible with short response times. Only significant changes are recorded, as defined for each variable, but time resolution remains as short as the basic processing cycle, typically one

minute. In this way, hundreds of variables can have their minute-to-minute variations captured with rapid recall of a month or more of history with only modest bulk storage requirements. Older data are frequently archived to magnetic tape or removable disk packs for review as required.

Process data have many users

Early approaches to process historians necessarily addressed a single requirement, e.g., a daily production or yield summary. In order to satisfy several different users with different needs, a more complex historian is required. Some examples of these users are discussed below:

Undisputedly the most important user of process data treats the historian in a way very similar to the familiar strip chart. Today his chart appears on a color graphics CRT terminal in the wink of an eye. He can arrange any set of variables of interest, confident that the plots will be accurate, synchronized in time, and that the pen won't stop inking. Operators are usually focused on only a few key process variables. The time span, which is readily adjustable, is most often set for four hours, regardless of the time constants of the process. Operators will, however, look back to periods of good operation to find clues to current difficulties.

Foremen appreciate having their own "window" or terminal access to the historian so that they won't disturb the operators. This extra console is also very valuable during start-up or emergency situations. Foremen tend to look at longer time spans, comparing their shift's operation over several days or against other crews. Production supervisors and superintendents benefit from analysis of detailed data for entire accounting periods, usually a month or more. Once record rates or yields are schieved, the complete operating conditions can be used to obtain repeat performances.

The process engineer's use of a historian's function is the most varied. At least three distinct modes can greatly increase the engineer's efficiency: routine performance review, problem diagnosis, and process testing/debottle-necking. An engineer supporting a process must frequently review recent plant performance. With a computer-based historian, the task of scanning the dozens of variables in his area of responsibility for the previous day or weekend takes only a few minutes. Upon completion he can be confident that he did not miss anything of consequence. This review leads to problem diagnosis, a job that is often hampered by lack of information.

The flexibility of the historical display permits a time span that could vary from five minutes full screen to three months. Since the data consists of the actual events rather than averages, the time sequence of events can be seen. This, in turn, allows a much better opportunity for determining the actual cause of upsets rather than being misled by a symptom. In the third mode, the engineer performs the usual plant process and capacity studies. The test may be a designed experiment or an analysis of the process response to unplanned disturbances. In either case the historian permits him to prepare detailed data sets for statistical correlation, comparison with process simulations, or design flow sheets, etc. A major step forward from the traditional clipboard approach.

Maintenance support often requires much longer view than other users. Examples include plotting the history of a large compressor's vibration probes and bearing temperatures over a multi-month span. Catastrophic failures can thus be avoided. A similar use would monitor calculated heat transfer coefficients in all major heat exchangers on a unit, permitting the cleanout to be scheduled well in advance. Many instrument problems can also be detected in this manner, using crossplots of process and laboratory analyzers on the same streams.

Data-saving techniques

This list of users is not meant to be complete, and there are clearly reasons that others including research chemists,

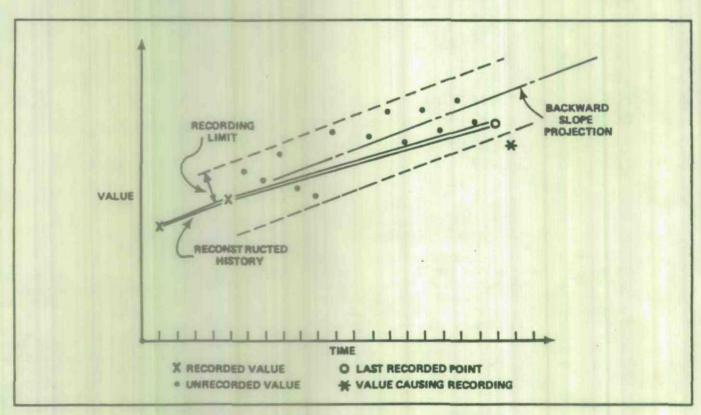


Figure 2. Backward slope algorithm.

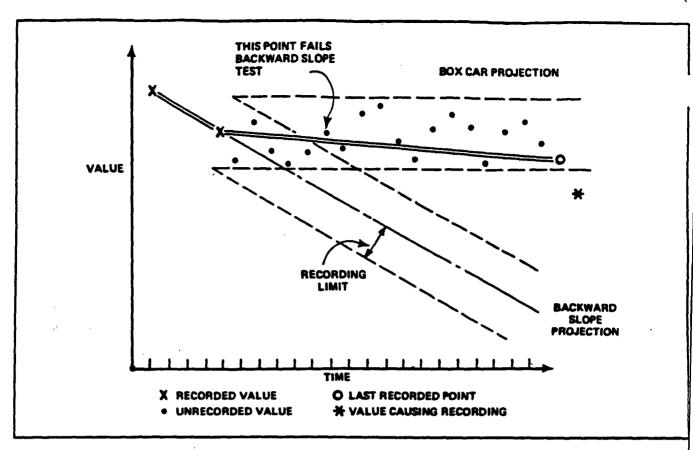


Figure 3. Combination algorithm.

marketing specialists, or design engineers need access to this process information. Present communication capabilities give the extra freedom to have some users remote from the plant site. An important benefit should be stressed; this is the improved communication among the different users. The operator now has solid proof of a process or equipment problem he went through on graveyard shift and can easily show it to the people who will have to solve it. While hard copy is available, most discussions among production, technical, and maintenance people take place around a console so that the historian can replay the problem from another angle.

The historian should be comprehensive. This means including all variables: direct measurements, derived calculations such as yield, and laboratory results. This approach assumes that if a variable is important enough to be in the computer, it should be recorded as well. Older panel board control rooms typically connected only 20 to 30% of all transducers to strip charts, primarily because of real estate limitations. No such restriction exists with modern computer hardware. In particular, the diagnosing mode demands that all the data be available. It recognizes that it is impossible to know ahead of time what information may be the vital clue. Experience with numerous troubleshooting sessions proves that seemingly unimportant transducers have been the key to major savings. This benefit frequently leads to a 20% growth in instrumentation connected to the process computer.

The parameters that determine the design of a process historian are straightforward. The volume of data will be a function of the number of variables recorded, the frequency of recording for each variable, and the total time span desired. Even for a modest-size process, this total can become a very large number. Other factors that become important are the desired retrieval and display time and the added computer load required to handle this added function. Many engineering tradeoffs are possible.

A satisfactory design for many situations involves a called snapshot approach. The total storage requirements can be significantly reduced by two routes: record only s limited subset of the total variables, say 30%; and store only 10 minute averages rather than the minute-to-minute readings. This combination would need only 5% of the space the full detail would require and could handle many accounting tasks quite well.

Computer load to store the data would be equally modest but retrieval would be slow since most of the files would be read back in and the selected variable taken out of each snapshot. Most implementations of this type permit a reselection of recorded variables with varying degrees of difficulty. Long-term storage might consist of printed log or some machine readable media such as floppy disks. Fo some applications, this will remain an adequate solution.

Data compression

As the requirements for the historian increase, the simpler techniques are no longer adequate. Retaining minute-by-minute readings for a month on a 1,000-variable system would require 45 million entries, more bulk storage than many process computers use for all purposes. Recognizing that there are long periods of operation in whice variables are either constant or moving in a predictable path, techniques of data compression can be utilized ver effectively.

Because data compression results in recording point that are no longer at equally spaced time intervals, each value must be stored with a date-time tag. For a computer, this can be done with eight bytes: four byte the real number value expressed in engineering units are two bytes each for integer codes of the date and time. In the case, the technique doubles the storage requirements preadings so that the data compression ratio must be great than 2:1 to be effective. Data compression is defined as the

number of values processed at equal time intervals which resulted in single recorded value. For a system processing variables at one minute intervals, a 30:1 data compression ratio would mean that each variable was being recorded

once each half hour on the average.

The data compression ratio is a crude index that reflects the overall operation of the historian. In practice, the amount of storage for each variable (an inverse function of the data compression efficiency) usually resembles a Gaussian distribution. Some variables can be characterized for a given time period with only one or two blocks of storage, e.g., lab results that are only obtained once or twice a shift. Very active variables such as flow rates often require 100-200 blocks to cover the same time. (A block corresponds to a disk sector or 512 bytes.) The majority of the variables could then follow in the range of 20 to 40 blocks.

It is not unusual for the storage requirements to change by two orders of magnitude from the most active to the most static on a single process. Not only does storage demand vary from variable to variable, it can vary significantly with the state of the process. Obviously, recording demands are heavy during start-ups or periods of upsets. Since the total memory available for historical purposes is usually fixed, this means the on-line time span contracts somewhat to reflect the temporarily decreased data compression ratios. As the plant lines out, the available

time span increases again.

Use of data compression requires that two choices be made for each variable: a recording limit and an algorithm to make the recording decision. The recording limit is most often selected to match the transducer's inherent accuracy. e.g., 1% of span or 0.5°C for thermocouples. This avoids recording measurement noise but captures true process changes. In a few cases, a recording limit of zero may be used to force recording of all measurable changes.

Selecting effective algorithms

While data compression algorithms may be quite complex, such as those used in space satellite communications (2,3), several straightforward techniques produce excellent results. Three of the algorithms that are discussed below have proven themselves in several years of use. The degree of computational complexity is an engineering tradeoff; the computation must be performed for each variable each time it is processed. Consequently, algorithms which achieved higher data compression ratios might not justify the additional computational load. Increasing capabilities in process computers will provide an incentive to use more sophisticated methods.

These three algorithms developed in an evolutionary manner. Early implementations used computers with very limited bulk storage, and there was a strong desire to record a time period of at least two or three days, thereby allowing review of a weekend's operation. Initial experiments with the Box Car showed it to be quite effective. The Box Car algorithm records when the current value differs from the last recorded value by an amount greater than or equal to the Recording Limit for that variable. Many processes are fortunate enough to run for long stretches of stable opera-

However, it became apparent that the Box Car did not always obtain high data compression ratios. A classic case is that of a large tank slowly filling. The Box Car algorithm will dutifully record each 1% of level, even though the entire change could be just as accurately described by a straight line connecting the start and end of the filling. Even continuous processes experience transitions from one rate to another, and, of course, batch operations are described in time as a series of ramping changes. The use of the Backward Slope demonstrated that this behavior could be accurately captured with significantly higher data compression ratios than the Box Car. (Computational

details of the algorithms are given in the Appendix). The Backward Slope uses the last two recorded values to predict the trend of the variable in the future.

In use, the Backward Slope did not always produce better results, i.e., higher data compression. Noise sometimes caused the projected slope to be meaningless. For these variables, the Box Car remained the best choice. This affirms that with noticeable noise the best estimator of the slope is zero. Having two algorithms helped, there still remained the problem of selecting which algorithm was best for a particular variable. This was difficult to know without actual observations, and it could vary for even a single variable depending on conditions. A level indication on a distillation column which is very noisy during an upset and stable otherwise is a common situation. This choice can be returned to the computer to handle on a dynamic basis for each variable individually. The result is the third algorithm, labeled the Combined Box Car and Backward Slope. It applies both criteria until both fail.

As applied in actual processes, there are several factors which influence performance. These include the type of process, the number and type of variables monitored, and, most importantly, the approached used to select algorithm types and recording limits. Someone who sets all thermocouple recording limits to 0.1°C will see little benefit from data compression. Review of several systems has shown that data compression ratios in the range of 30:1 are easily obtained and results of 80:1 to 100:1 have been realized

without loss of meaningful information.

Display of historical information

Having put this much effort into recording process histories, there must be some way to access it. One of the best is by presentation on a color graphics CRT terminal. Fast response time is essential, since this information may be needed for decisions in emergency situations. Even in routine operation, it should be easy to scan through large quantities of data quickly. One property of a display screen is especially important: high resolution. Having gone to the trouble to preserve the details of variable movement, it doesn't make sense to throw it away by low resolution displays. Hard copy devices such as plotters can be useful, but the dominant method of access is by time-series plots

on display screens.

The equipment and programming techniques used to provide graphics displays will vary from system to system, but some comments can be made about the man-machine interface. Access to the historian needs to be as flexible as possible. A user must be able to rapidly request the display he needs. This means control of the variables displayed, the time span and the scale for each variable plotted. In order to observe interactions, at least two variables must be plotted together and more than two can be very helpful. Four simultaneous variables is a good compromise between useful information and confusing displays. The time span must be easily changed. It is useful to "flip" through data sets with long time periods and then "zoom" in on interesting details. In the same way, expanding the scale can help define subtle shifts and take full advantage of the instrumentation's inherent accuracy.

All this flexibility can lead to a console that is difficult to use or, even worse, is ignored. Use of single pushbuttons to provide common commands, e.g., setting standard time intervals such as 1, 2, 4, and 8 hours is much simpler to use than a typed command of several characters. Similarly, preselecting groups of variables to display together is very helpful. The ability to assemble any combination is always available. In practice, operators view almost all their electronic "strip charta" with a single key stroke which can lead them quickly through a predefined view of the recent

history of the process.

It is very difficult to describe this method of viewing the

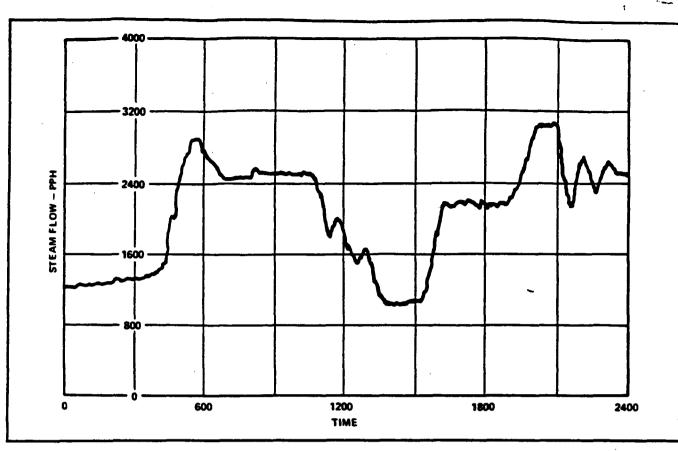


Figure 4. Steam flow rate.

process, unless you are observing the consoles. Typical displays are shown in Figures 1 to 4. The human mind has a remarkable facility for extracting key observations out of the thousands of data points displayed in this manner. Frequent use of this view of a process leads to mental models of these patterns just as operators remember dial positions of panel board instruments. Operators become conscious that "things don't look right" without going through a structured analysis. Other uses for this historical data are being developed, but visual screening by the people associated with a plant is certain to remain a very important justification.

Bulk storage management required

The historian depends on a substantial amount of fast access bulk storage, e.g., disk drives, as part of the process control system. Some features are important to the proper operation of the historian.

Typically the historical data base is organized as doubly linked, circular lists of disk blocks or sectors. Each block will contain several readings and their date/time tags, e.g., 60 pairs. Each variable has its own linked list which is found in a directory pointing to the head and tail of each linked list. History is thus sorted by variable as it is recorded. This is a major factor in fast response displays. This technique can make possible the display of a single variable's history for eight hours in 2 to 4 seconds, and a set of four variables in only 4 to 8 seconds. Very noisy variables with low compression ratios will require somewhat more time.

The data compression and sorting have a synergistic effect on response time. Assuming a 30:1 data compression ratio for a given variable, the actual storage would be 15:1 due to the date/time tag. If the data were recorded every minute, four disk transfers would be required for an eighthour display and transmitting it the screen would consume two seconds at 9,600 baud (assuming four bytes per plotted

point). Compression would require only one or two disk transfers (averaging 1.5 because data may be shared between two blocks) and transmission time of only 0.07 seconds.

The linked list for a variable may be entered at either end. Displays most often use the most recent data and archiving functions access the oldest. Some data are entered after a delay. This feature is needed because laboratory results and other manual readings are not available in real time but are an important part of the process history. These data are time tagged with its actual sample or measurement time, not the time it was entered.

A bulk storage management function is important; this program collects and archives history for long-term storage to free up space for the new data that are being collected. It attempts to keep the maximum time period available online that its file size will permit. If the archiving is temporarily lost due to equipment failure, the historian will continue to operate satisfactorily by writing over the oldest data in the system. Several utility functions have been developed to repair problems such as bad disk blocks, broken links, incorrect times, etc. So far, no one has found a totally acceptable answer to the Fall change from daylight savings to standard time! Other related functions store and retrieve old data when required. When an old set is read back into the computer, it is relinked to the recent information thereby becoming accessible in the normal way. In this manner, plots of key variables can be prepared for time spans as long as a year or more.

Some tools are required to "tune" the historian. Some noisy variables may be wasting the resources of the machine without providing useful information. The top few variable which have low compression ratios should be periodically reviewed to determine if they require that volume of data to accurately reflect their movement. Changes in recording rate with respect to the rest of the variables may signal either an instrumentation failure or a process change.

In summary

The process historian has demonstrated major benefits in use over several years with varied processes. Nevertheless, it has also proven difficult to describe to potential users. There are at least two reasons for this. The first relates to the need to observe a real system in operation. The historian has the power to adapt to a wide range of users, but actual hands-on experience is needed to convince people of this fact. A second factor is the concern that a substantial data compression cannot be achieved without sacrificing the accuracy of the regenerated curves. Confidence is sometimes only achieved with actual use.

A major advantage of data compression for a process historian is that it can be the difference between making the function feasible or not. The historian's usefulness has been shown to greatly increase when all variables are recorded and the on-line storage consists of many days. This relates to the need to analyze problems, which are both complex and which are not immediately detected. Feasibility can be measured several ways. One is equipment cost, both investment and maintenance. While it is cost-effective to devote a disk drive to this function, eight or 10 drives are not realistic. Among other things, floor space adjacent to control rooms is very expensive. These cost factors carry through to other items such as storage of archival material.

Feasibility is also related to responsiveness. If information is not readily available for real time decisions, its value is greatly diminished. Response time is directly related to the reduced volume and presorted condition. Users will not request information frequently, if long delays result. Some historians plot several thousand time histories each day.

The problem analysis or troubleshooting ability has already been cited. This aspect is particularly important during startup of a new or expanded facility. The historian can greatly accelerate the "learning curve" resulting in payouts for the entire process computer system during this phase alone. In one case, 18 interlocks occurred to a reactor during its initial operation of three weeks. In every case, the true source of the interlock was detected and corrected.

It achieved excellent performance following this startup period; without a historian, the reacter would have restarted with no proven explanation of some of the interlocks. When actual problems are solved, unit utility frequently improves with accompanying safety benefits. The benefit of having all the data accurately captured cannot be overemphasized. All too often, an analysis cannot be made because too little is known about what really happened.

Our experience to date with process historians has been very encouraging. It suggests that it must be comprehensive and responsive to be fully effective. To date, we have been able to achieve significant cost savings in the installed equipment and, more importantly, obtain better process insight. We have seen that as the historian's capabilities increase, it can serve a variety of users with quite different needs, rather than the limited, dedicated approach that is often employed. Certainly there are many ways that the current technology of process computers can be expanded and enriched. We believe that process historians will become an increasingly important reason for installing a computer on a process.

Acknowledgments

Harold L. Sellars' work on the historian was done while at Biles and Assoc., Inc., Houston, Texas under the contract with E. I. du Pont de Nemours & Co., directed by John C. Hale. Randolph S. Knipp, Du Pont, supervised the initial installation.

Literature cited

1. Crowder, R. S., Instrumentation Techn., 18, 1, p. 58 (January, 1971).

 Davisson, L. D., "Data Compression Using Straight Line Interpolation," IEEE Trans., it-4. No. 3, p. 390 (1968).

Appendix: Data Compression Algorithms

Box Car Algorithm. This method records data when a value is significantly different from the last recorded value, Figure 1.

If $|V - V_R| \ge H$, record the previous value processed, not the current value which caused the triggering of the recording. Recording is accomplished by setting:

$$T_R - T_L$$
$$V_R - V_L$$

Backward Slope. In this case, the decision is based on a projection defined by the slope S and the last recorded value, Figure 2.

$$|V - (V_R - S(T - T_R))| \ge H$$

Recording is accomplished in the same manner as for the Box Car, and a new slope is calculated which is derived from this newly recorded point and the recorded value immediately prior to that.

Combination Box Car and Backward Slope Algorithm. This method combines the two above by using an adaptive parameter, P. P is initialized to zero and remains there as long as both of the tests are passed. If the Backward Slope test fails, P is set to one, and the method reverts to the Box Car until a recording is made. The algorithm is then reinitialized by setting P to zero. If the Box Car fails first, P is set to 2, and only the Backward Slope is used until a recording is made. If both tests are failed while P is zero, recording is performed, and P remains at zero, Figure 3.

Notation

V - current value of variable

 V_L - last current value on previous processing cycle

 V_R - most recent recorded value

T - current time

 T_L - time of previous processing for this variable

 T_R - time matching most recent recorded value

H - recording limit parameter

S - projected backward slope - $(V_L - V_R)/(T_L - T_R)$

All Vs and Hs are in standard engineering units such as °C or kg/h. The Ts are time intervals that imply a date/time identification so that time intervals of longer than a day can be accommodated. In general, H, the recording limit, is adjustable on a variable-by-variable basis.



J.C. Hale, consultant manager for on-line systems in the Engineering Dept. of E.I. Du Pont de Nemours & Co., has had a variety of assignments involving process computers. He earned his B.E. degree at Vanderbilt Univ., and his Sc.D. at the Univ. of Virginia.



H.L. Sellars, an instructor at Southwest Texas State Univ., earned his B.S. and M.S. degrees in mathematics at the Univ. of Alabama. An active industrial consultant, he specializes in computer control software, system design, and project management. He has had more than 15 years of experience in computer control of chemical and refining processes.

P.73

APPENDIX E

APPENDIX E



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY Office of Air Quality Planning and Standards Research Triangle Park, North Carolina 27711

MAR 3 1992

Mr. Larry L. Thomas
President
The Society of the Plastics Industry
1275 K Street, N.W., Suite 400
Washington, D.C. 20005

Dear Mr. Thomas:

This is in response to your January 21, 1992 letter to Mr. Rosenberg requesting clarification of the definition of Polycyclic Organic Matter (POM) as listed in Title III, Section 112(b)(1), of the Clean Air Act Amendments of 1990 (CAAA).

As you mentioned in your letter, historically the working definition of POM has been that complex mixture of compounds which is formed during organic combustion and pyrolysis processes. However, POM, if broadly defined in Section 112(b), could potentially include many chemicals not associated with combustion or pyrolysis such as the benzene-based polymers and plastic related compounds. Several compounds that could be classified as POM are listed individually as specific hazardous air pollutants, (i.e. 2,3,7,8-Tetrachlorodibenzo-p-dioxin). Consequently, if specific, non-combustion or non-pyrolysis chemicals meeting the current definition of POM are discovered to be hazardous air pollutants in the future, such pollutants could be individually listed rather than included in the general POM category. The intent of not characterizing individual compounds in the POM compound category is further supported by the statutory language which precludes petitions for unique chemical substances from the POM compound category. This language indicates that unique, specific, chemicals would not be identified within this mixture. For the present, the definition will remain as it appears in the CAAA. The use of this definition, however, will continue to emphasize emissions from combustion and pyrolysis activities.

We are seeking to codify the list of pollutants under Section 112b and plan to identify this issue for comment. The use of this definition, however, will continue to emphasize emissions from combustion and pyrolysis processes. As you noted in your letter, the production of plastics and the manufacture of plastic products are currently included on the source category list but not on the basis of emitting POM. They are, however, included on the source category list as emitting other pollutants listed under Section 112(b)(1).

If you have a specific chemical compound in mind for which you would like clarification or if you would like to discuss the interpretation of POM and the implications under the Clean Air Act of 1990, please call Dr. Nancy Pate in the Office of Air Quality Planning and Standards at 919-541-5347. The ongoing efforts of the plastics industry to recycle plastic, reduce emissions and develop environmentally sound operation management practices are appreciated and encouraged.

Sincerely,

Director

Office of Air Quality Planning and Standards

APPENDIX F



Texas Eastman Division P.O. Box 7444 Longview, Texas 75607-7444 903.237.5000

April 13, 1993

Ms. Karen Fidler Chemical Manufacturers Association 2501 M Street, NW Washington, DC 20037

Dear Karen:

Re: Assessment of Low Flow Cutoff - Attachment for CMA Comments on the HON

EPA's determination of a low flow concentration limit is described in docket A-90-19, item II-B-272. EPA made the determination from an evaluation of 1266 vent stream points in the HON database (the later database not available in the docket for this rulemaking). EPA determined the minimum positive flow rate in the database for any vent stream with a TRE value less than 1 as 0.005 scmm.

Not having the database to review, an alternative analysis was undertaken to assure the 0.005 scmm cutoff was not totally inconsistent with the proposed TRE equation and coefficients. The attached analysis indicates the TRE equation, when highly biased with simplifying assumptions, would categorize all flows as Group 2 for flowrates less than 0.001 scmm. In addition, the analysis agrees with the EPA analysis that the flare coefficients determine the cutoff value rather than the other coefficients.

It is concluded therefore that the 0.005 scmm cutoff is consistent with TRE equation within the accuracy of this assessment method.

Yours truly,

[/]J. L. Woolbert, P.E.

Principal Chemical Engineer Environmental Affairs

L010JLW3.tjb



P.78

Attachment 1

Analysis of Low Flow Cutoff Consistency With TRE Equation

$$TRE = \frac{1}{E_{HAP}} [a + bQ_s + cH_t + dE_{TOC}]$$

Objective:

To determine EPA's flow value cutoff level of 0.005 scmm to be utilized for Group 2/non-applicability determination of the HON Process Vents provisions is consistent with TRE coefficients proposed December 31, 1993.

ANALYSIS:

Assumptions:

- 1. Ignore Q_s term because b is always positive (> 0) and will always bias TRE numerator toward Group 2:
- 2. Assume entire flow is HAP compound to bias analysis toward Group 1.
- 3. Assume entire flow
 - a. is TOC (i.e. $E_{TOC} = E_{HAP}$) where d coefficient is negative
 - b. is non-organic (i.e. $E_{TOC} = Zero$) where d coefficient is positive

to bias analysis toward Group 1.

- 4. Assume vent stream net heating value
 - a. Maximum of $H_T =$ where c coefficient is negative, and
 - b. is $H_T = 0$ where c coefficient is positive

to bias analysis toward Group 1.

Specific Evaluations of Reduced TRE Equation

Case I - Non-Halogenated Flare

(Existing)
$$TRE_{FLARE} = \frac{1}{E_{HAP}} [2.902 - 1.153 \ X \ 10^{-2} \ H_T - 1.100 \ X \ 10^{-3} \ E_{HAP}]$$

(New)
$$TRE_{FLARE} = \frac{1}{E_{HAP}} [0.5276 - 2.098 \times 10^{-3} H_T - 2.000 \times 10^{-4} E_{HAP}]$$

Case II - Non-halogemated Thermal Incinerator
0 Percent Heat Recovery

(Existing)
$$TRE_{INC_{10}} = \frac{1}{E_{HAP}} [2.238 - 1.739 \times 10^{-3} E_{HAP}]$$

(New)
$$TRE_{INC,\Theta} = \frac{1}{E_{HAP}} [0.4068 - 3.162 \times 10^{-4} E_{HAP}]$$

Case III - Non-halogenated Thermal Incinerator 70 Percent Heat Recovery

(Existing)
$$TRE_{INC,70} = \frac{1}{E_{HAP}} [3.778]$$

(New)
$$TRE_{INC,70} = \frac{1}{E_{HAP}} [0.6868]$$

Case IV - Halogenated, Thermal Incinerator and Scrubber

(Existing)
$$TRE_{INC,SCRB} = \frac{1}{E_{HAP}} [5.992 - 2.653 \times 10^{-3} H_T]$$

(New)
$$TRE_{INC,SCRB} = \frac{1}{E_{HAP}} [1.0895 - 4.822 \ X \ 10^{-4} H_T]$$

For terms with E_{HAP} in numerator, it is apparent when dividing each term by $1/E_{HAP}$, this term is a minor term when TRE is approximately 1; therefore, these terms are deleted from the equations in further analysis.

The most stringent of the above pairs of equations are the "(new)" equations as follows:

Case I

$$TRE_{FLARE} = \frac{1}{E_{HAP}} [0.5276 - 2.098 \ X \ 10^{-3} \ H_T]$$

Case II

$$TRE_{INC,0} = \frac{1}{E_{HAP}} [0.4068]$$

Case III

$$TRE_{INC,70} = \frac{1}{E_{HAP}} [0.6868]$$

CASE IV

$$TRE_{INC,SCRB} = \frac{1}{E_{HAP}} [1.0895 - 4.822 \ X \ 10^{-4} H_T]$$

Note: For given values of H_T and E_{HAP}, Case I is more stringent than Case IV and Case II is more stringent than Case III. The resulting assessment is then to determine the corresponding flows for

Case I

$$TRE_{FLARE} = \frac{1}{E_{HAP}} [0.5276 - 2.098 \ X \ 10^{-3} H_T]$$

and Case II

$$TRE_{INC,0} = \frac{1}{E_{HAP}} [0.4068]$$

Substituting worst-case heating value (see calculation in Attachment 2) into Case I equation result in

$$TRE_{FLARE} = \frac{1}{E_{HAP}} [0.5276 - 2.098 \ X \ 10^{-3} \{147\}]$$

$$= \frac{0.2192}{E_{HAP}}$$

Therefore, for purpose of the analysis, the flare example would be expected to yield the lowest flow cutoff value to guarantee TRE > 1 for all vents subject to the TRE equation that were indeed (TRE > 1) Group 2.

At TRE = 1

$$E_{HAP} = 0.2192 \ Kg/hour$$
and, $Q_S = K_2 \frac{RT}{MWP} E_{HAP}$
where $K_2 = \frac{1000g}{Kg} X \frac{1m^3}{10^6 cm^3} X \frac{1 \ HOUR}{60 \ MIN}$.

$$R = \frac{82.057 \ atm \ cm^3}{^{\circ} \ K \ gram - mole}$$
$$T \ [=] \ ^{\circ} \ K$$
$$P \ [=] \ atm$$

Thus,

$$Q_{S} \left[\frac{m^{3}}{\min} \right] = \frac{(1.667 \ X \ 10^{-5})^{-}(82.057)(293.16)(0.2192)}{MW \ (1)}$$

$$Q_{S} = \frac{0.08790}{MW}$$

Average molecular weight of VOC mixture in Net Heating Value Calculation ≈ 72.

$$Q_s = \frac{0.08790}{72} = 0.0012 \ m^3/\text{min}$$

Attachment 2

Estimation of Worst-Case Net Heating Value

Procedure: Add in a cumulative sequence the net heat contribution from successively lighter bydrocarbons at saturated conditions until the sum total pressure is 1 atm. at STP (20°C).

			(2)Net Heat of Con	nbustion(KCal/mole)
Assumed	STP at 20°C			Contribution to
TOC Compound	Vapor Pressure ⁽¹⁾	Partial Pressure	TOC	<u>Mixture</u>
•	4.60	1.20	1600.04	2.70
decane	1.30 torr.	1.30	1632.34	2.79
nonane	3.46 torr.	3.46	1474.90	6.71
octane	10.5 torr.	10.5	1317.45	18.20
heptane	33.0 torr.	33.0	1160.01	50.37
hexane	10\s torr.	108	1,002.57	142.47
pentane	375 torr.	375	845.16	417.20
butane	1476 torr.	(760-531.26)	687.982	207.06
propane	6396 torr		530.605	·
ethane	30918 torr.		372.820	
	TOTAL:	760	TOTAL:	844.62

 $H_T = (1.740 \ X \ 10^{-1})(844.62) = 147 \ MJ/SCM^{(3)}$

¹CRC Handbook of Chemistry and Physics, 53rd Edition, (CRC Press, Robert C. Weast, EJ., Cleveland, Ohio 44128) Pp. D-151 - .

²Net heat of combustion from <u>Chemical Engineer's Handbook</u>, Perry and Chilton, 5th Edition (McGraw-Hill Book Company, New York, New York) Pp. 3-145, 3-146.

³Modified equation at 57 FR 62700 by 10⁶/ppm multiplication

APPENDIX G



CHEMICAL MANUFACTURERS ASSOCIATION

Ms. Sheila Milliken
Emissions Standards Division
Standards Development Branch (MD-13)
U.S. Environmental Protection Agency
Office of Air quality Planning and Standards
Research Triangle Park, NC 27711

Dear Ms. Milliken:

Thank you for the opportunity to discuss a calculation-based TRE cutoff for process vents on August 5. A copy of CMA's analysis, which we discussed, is attached. To summarize our discussion, the enclosed analysis proposes an engineering assessment of the conditions that would reasonably be expected to occur in actual operation which would result in the lowest calculated value of TRE. Using this basis, process variability was excluded from further effect in the analysis (see Handout 1 enclosed.)

Within the expected accuracy of engineering estimates, the enclosed analysis indicates that a TRE cutoff value of 3 will capture all Group 1 vents in the EPA BID draft with the exception of a single high flow, low HAP concentration vent. CMA suggests EPA may wish to consider an alternate cutoff value for this type of vent, or alternately, to exclude high flow, low HAP concentration vents from the calculation-based alternative. CMA did not suggest alternative cutoffs for this single vent in the database because one data point did not provide a sufficient database for establishing either a TRE cutoff or "high" flow/"low" concentration breakpoints.

The practical value in establishing this calculation-based cutoff is to provide relief to limited testing resources from the TRE testing determination procedure for those process vents that are obviously Group 2. The degree to which relief is provided is highly dependent on the value of the cutoff selected.

A cutoff value of 3 will provide the requisite assurance of proper Group 1 vent identification in the HON. Precedent exists in NSPS regulations for a value of four (4) [40 CFR 60.610 (c) and 60.614(f)(2)]. The enclosed rationale supports the conclusion that a value of 3 would be appropriate for the HON and is consistent with TRE cutoff values previously established by the EPA. On the other hand, a cutoff value of 8, as suggested in the pre-proposal, would significantly increase the number of Group 2 vents that would have to undergo testing and would erode the benefits of a calculation-based approach. (See Enclosure 1)

We hope this analysis is helpful in providing a scientifically defensible basks for proposing a reasonable calculation-based TRE cutoff value. If you have any questions upon review of this information, please call myself or Annette Stanley at (202) 887-1370 or (202) 887-1308 respectively.

Sincerely yours,

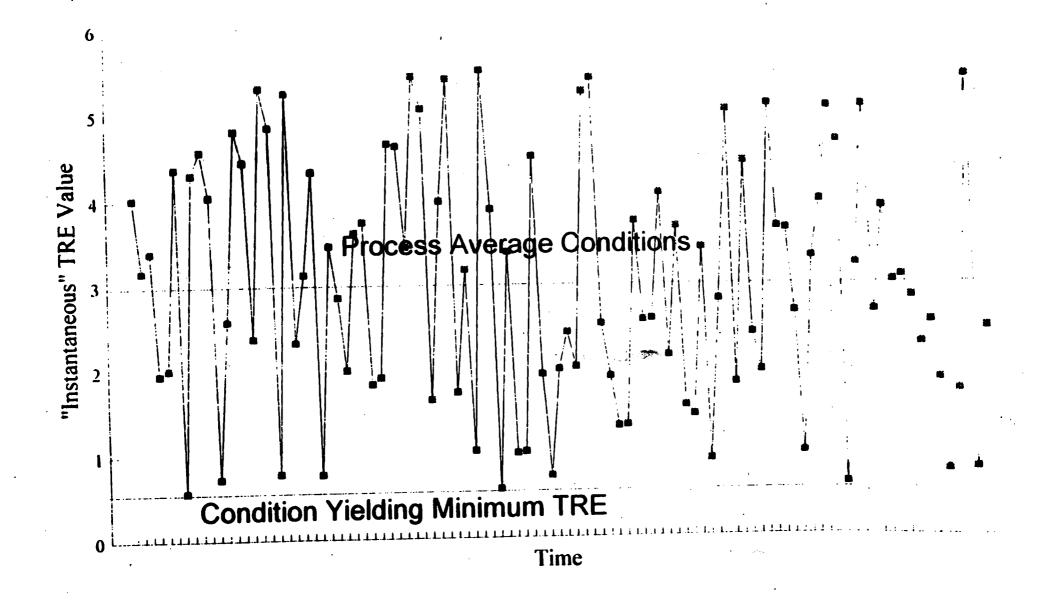
Amy Meyers

Manager, Air Programs

cc: L. Evans

J. Meyer

R. Rosensteel



Handout 1

Enclosure 1

X-Value Effects on Predictability of Group 2 Status for Group 2 Vents in EPA October 1991 Draft BID

	TRB-I-3	70.256	TREX=0
1. Vent expected to calculate Group 2	7	7	•
2. Vent expected to calculate false Group 1 or Group 2	10	•	5
3. Vent expected to calculate false Group 1	5	7	11
TOTAL GROUP 2 VENTS	22	22	22

Comment:

This table is based on the information for the 22 non-Halogenated vents in the October 1991, Draft BID for the HON, Vol. 1C, Tables 2-2 through 2-5. It is assumed the information in the BID represents the "true" values for calculating TRE values for the vent. The status groupings above indicate, based on accuracy ranges for engineering estimates of the "true" values and a TRE cutoff value of X, whether the estimated TRE for the vent would

- 1. always calculate <u>above</u> the TRE x-value; i.e., accurately identify the Group 2 vent as Group 2.
- 2. calculate above or below the TRE x-value depending on where TRE input variables fall in the estimated error range; i.e., sometimes result in correct Group 2 identification but at other times result in a false Group 1 identification.
- 3. always calculate <u>below</u> the TRE x-value; i.e., always incorrectly identify the Group 2 vent as Group 1.

ANALYSIS SUPPORTING CALCULATION-BASED TRE CUTOFF FOR THE HON

Introduction

The TRE determination procedure in the December 24, 1991, pre-proposal draft of the HON §63115(b)(1) and (2) requires measurement of flow and composition of all process vents. Resource requirements and costs in time and material can be substantial for measurements at a large number of vents. While measurement may be a reasonable requirement for vents with TRE values close to the Group 1 - Group 2 breakpoint (TRE = 1) in the HON, such a requirement overburdens limited resources when other, less burdensome assessment methods can assure a vent is Group 2 (i.e., the vent does not require control equipment application).

Engineering estimated quantities may reliably be used to determine a vent's Group status instead of measured quantities when information from best engineering estimates predict a TRE > 3 and when high flow/low concentration vents are excluded from the engineering estimate option. This conclusion is derived from the accuracy that can reasonably be expected from best engineering estimates, quantified inaccuracy propagation through the TRE equation, and testing of the hypothesis with the process vent data in Volume 1C, Tables 2-2 through 2-5 of the October, 1991, draft BID for the HON. The details of this analysis are provided below.

Analysis Procedure and Basis

This analysis included the following tasks:

1. Specification of engineering estimate accuracy expectations for

TRE formula variable quantities.

- 2. Determination of error propagation relationship in TRE equation.
- 3. Calculation of TRE and Confidence Intervals for process vent data.

Specification of accuracy expectations for the variables in the TRE equation is based on best engineering judgement. The accuracy estimates and conversion formulas used in the analysis are shown in Table 1.

Variable accuracy is estimated on three separate bases corresponding to three ranges of the variable scale. The first range is the "high" variable range in which inaccuracies would be expected to be observable and easily judged from process experience. In this range, accuracies of engineering estimates should be within a fraction of the variable value. The second range is the "intermediate" variable range in which accuracies of engineering estimates should be within a few multiples of the variable value before inaccuracies would be expected to be observable from process experience. The third range is the "low" variable range in which accuracies of engineering estimates may only be within order(s) of magnitude of the actual variable value. In this range, inaccuracies in variable quantities may not be observable from process parameters.

The error propagation equation is derived in Appendix A. This analysis assumes the engineering estimates of the variable values are independent; e.g., estimating the values of E_{HAP} and E_{TOC} are done independently such that method inaccuracy in the estimate of one value is not also incorporated in the estimate of the other value. If engineering estimates of the variables are based on common base data or assumptions (e.g., E_{HAP} and E_{TOC} calculated

Table 1

Be	st Engineering Judge	ment of Engineeri	ng Estimate Accuracy(1)
TRE Variable	Related Estimate Variable	Key Estimate Variable Range	Accuracy Expectation in Range
E _{HAP} ⁽²⁾	HAP Concentration	25 - 100% 1 - 25% < 1%	 ± 10% of Estimated Value ± 2% Composition ± 1 order of Magnitude of Estimated Value
E _{TOC} (3)	TOC Concentration	25 - 100% 1 - 25% < 1%	 ± 10% of Estimated Value ± 2% Composition ± 1 Order of Magnitude of Estimated Value
H_{\scriptscriptstyleT}	H _T (BTU/SCF)	10 - Full Range > 0 - 10 0	± 200% of Estimated Value ± 1 Order of magnitude of Estimated Value + 10 BTU/SCF
Q _s	Q _s (scfm)	> 100 1 - 100 < 1	± 20% of Estimated Value ± 10 scfm ± 1 Order of Magnitude of Estimated Value

Notes:

- (1) Estimate Accuracy defined as 95% confidence (30) Boundaries of Estimated Quantities
- (2) E_{HAP} Error Estimated from Equation

$$E_{HAP\ ERROR} = E_{HAP,\ Expected} \times \frac{HAP\ Concentration,\ ERROR}{HAP\ Concentration,\ Expected}$$

(3) E_{TOC} Error Estimated from Equation

$$E_{TOC, ERROR} = E_{TOC, EXPECTED} \times \frac{TOC\ Concentration,\ Error}{TOC\ Concentration,\ Expected}$$

From common vapor liquid equilibrium data and H_T and Q, derived from VLE analysis), covariances of the variable quantities become important factors in the variance analysis. In general, positive covariances add to the magnitude of TRE variability while negative covariances will reduce this magnitude. Because of the significant additional complexity added by consideration of covariance, this analysis alternately treats the TRE variable estimates as independent and assigns large inaccuracy to the single variable estimates. Where process knowledge is utilized to estimate parameter bounds, it is believed substantial independence among the variable estimates is achieved; e.g., Q, estimated from volume displacement parameters of the process, visible plume velocity, or pressure drop calculation; H_T estimated from inert concentration, "typical component" content and "typical component" heat of combustion; E_{TOC} estimated as concentration at pressure and temperature conditions less inert concentration; and E_{HAP} calculated from VLE data and process conditions for specific HAP components.

The confidence interval of TRE estimates was calculated for the vents and model vents in Volume 1C, Tables 2-2 through 2-5 of the October, 1991 draft BID. Coefficients utilized in the TRE Equation were those for Existing Vent Streams, Table 1, Page 370 of the December 24, 1991, draft of the HON. Bases and intermediate calculations are included in Attachment B. Based on additional information provided by EPA, a distinction is made between halogenated and non-halogenated vents.

Analysis Results and Discussions

The results of the TRE confidence interval calculations are shown in Tables 2 and 4. Supporting information are shown in Tables in Appendix B.

Group 1 Vent Analyses

a. Halogenated Vents

Based on information provided by EPA, the draft BID vent database (Tables 2-2 through 2-5) contained three (3) Group 1 Halogenated Vents. Information provided in the BID only allowed variance estimation for one vent as shown in Table 2. This single vent would have a maximum calculated TRE of 1.42 with the variable accuracy parameters shown in Table 1. Therefore, with a calculation based TRE cut-off approach, capture of all halogenated Group 1 vents will occur with a calculated TRE ≤ 1.5.

b. Non-halogenated Vents

The distribution of TRE range maxima for Non-halogenated Group 1 vents in the BID database is shown in Figure 1. All but one of these vents would have calculated TRE values less than or equal to 3 with the variable accuracy parameters shown in Table 1.

Categorical Analysis of the non-halogenated Group 1 vent with calculated TRE maxima greater than 3 is shown in Table 3. Capture of all non-halogenated Group 1 vents under a calculation based TRE cut-off approach is achievable with the following specification.

Table 2
TRE Confidence Intervals
Group 1 Vents

HALOGENATED

Table	Product	TRE	TRE Min Est	TRE Max Est
2 - 4 2 - 5	Dehydrohalogenation	0.1282 0.2558 0.4214	-0.5731	1.1217
	NON-HALOGENATED		•	
Table No.	Product	TRE	TRE Min Est	TRE Max
2 - 3 2 2 2 5 5 3 2 3 4 3 5 3 4 5 5 5 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Methyl Methacrylate Dimethyl Terephthalate Ethylene Oxide Acrylonitrile Maleic Anhydride Air Oxidation Distillation V Acetic Acid Phthalic Anhydride Butadiene Styrene Methanol Formaldehyde Nitrobenzene Vinyl Acetate Distillation NV Cyclohexanone/cyclohexane Ethylbenzene Dehydrogenation Nitration Methyl Ethyl Ketone Ethyl Acrylate Actaldehyde Ethylene Glycol Mono Ethylacetate	0.0062 0.0340 0.0635 0.1829 0.0751 0.1075 0.0649 0.0685 0.1059 0.0753 0.1084 0.0999 0.1347 0.1350 0.1377 0.1623 0.1872 0.2263 0.2405 0.3093 0.3865 0.4468 0.5417 0.6281 0.0647		1.0063 1.0653 1.3279 1.1878 1.1168 1.5337 1.0654 1.0687 1.1067 1.1523 1.1170 1.1600 1.6781 1.1576 1.2244 1.1873 1.2740 1.3130 1.3220 2.3046 1.8777 20.0305 1.6966 3.0022

FIGURE 1
Distribution of TRE Confidence
Interval Maxima - Group 1 Vents

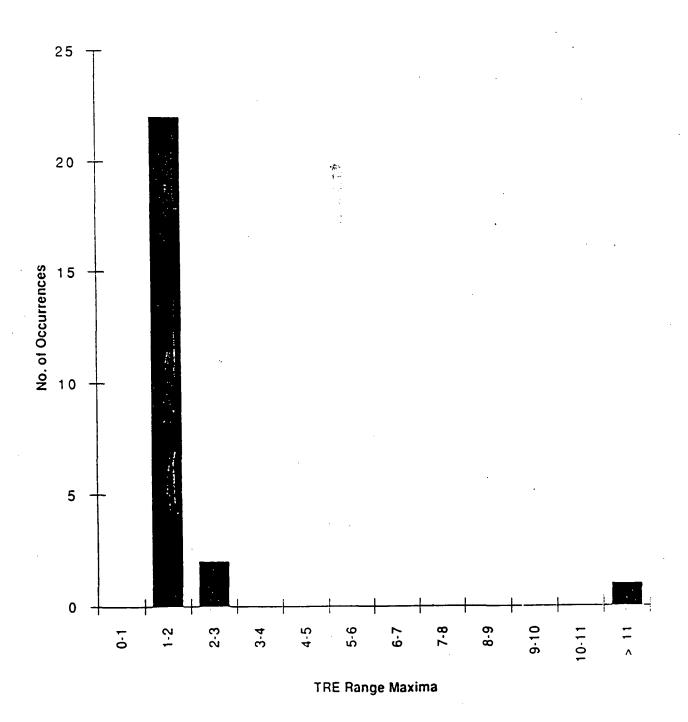


Table 3

Process Product	TRE Max	Flow ⁽¹⁾	Composition ⁽²⁾	Heat Content ⁽³⁾
Acetaldehyde	20	Н	L	L

Notes:

- (1) H = High Value; scfm > 100 M = Mid Value; 1 < scfm < 100 L = Low Value; scfm < 1
- (2) H = High Value; % HAP, TOC > 25 M = Mid Value; 1 < HAP, TOC < 25 L = Low Value; HAP, TOC < 1
- (3) $H = High Value; BTU/ft^3 > 200$ $M = Mid Value; 10 < BTU/ft^3 < 200$ $L = Low Value; BTU/ft^3 < 10$

- Require sampling on process vents with "high" flow rates
 and with "low" HAP and TOC compositions or establish
 an alternate TRE cutoff for such vents.
- 2. Require sampling on process vents with engineering-based TRE estimates less than or equal to 3.

Group 2 Vent Analyses

Given the above outlined constraints required to assure accurate classification of all Group 1 vents through engineering estimate methods, the next consideration is the effects of these constraints on Group 2 vents.

a. Halogenated Vents

Table 4 shows the halogenated Group 2 vent population from vents listed in the draft BID. Out of 7 total halogenated Group 2 vents, the minimum expected TRE values are greater than 1.5 for three (3) vents; for these vents, engineering estimates alone would suffice to correctly identify the vents as Group 2. The remaining four (4) vents would be variously categorized as Group 1 or Group 2 based on the estimated TRE value. Where the TRE estimate is less than 1.5, a false Group 1 indication would have to be confirmed with actual testing. A tabular summary of this information is shown in Table 5.

b. Non-halogenated Vents

Table 4 shows the Non-halogenated Group 2 vent population from vents listed in the draft BID. Out of 22 total Non-halogenated Group 2 vents, the minimum expected TRE values are greater than 3 for 7 vents; for these vents, engineering estimates alone would suffice to correctly identify the vents as Group 2. An additional 5 have maximum expected TRE values less than 3; engineering estimates would incorrectly identify these vents as members of the Group 1 category 100% of the time. Subsequent testing would be required to demonstrate their appropriate classification as Group 2 vents. The remaining 10 vents would be variously categorized as Group 1 or Group 2 based on the estimated TRE value. Where the

Table ; TRE Confidence Intervals Group 2 Vents

HALOGENATED

Table No.	Prod	유	Min	Ŋ
 - -	Chlorobenzene	1 00	1 666	1 0
- 1	genat	1.7435	0.7296) -f 0 (~ 0 () 1 ()
ŀ	thyl Chlori	.501	. ± 38	
ı	hylene Dichl	.215	9.5	.238
ı	rchloroeth	.286	.286	.286
1	logen	.916	.895	.936
1	Hydrohalogenation	.175	.401	.949
	NON-HALOGENATED			
4	Vegerlag		: :	:
) 10 (7)		ti O.F.	IRE NIN	
	10001		S)	ו ר
	erephthalic Aci	11	-46.181	417.8
2-5	Hydrogenation	87	(-	∞
J	enze	86	.230	.342
j	atal	286	.230	.342
ı	itrobenze	59	.078	.640
J	ydrodimer	.384	.192	.576
J	diponitri	384	.192	.576
1	sterificat	.475	.392	.342
1	lkylatio	34	.244	.112
1	ondensati	.214	.439	.868
ı	erephthalic	. 246	.662	.830
1	ener	.493	.692	.294
1	lin	.339	.658	.337
1	Hydroformylation	.891	.920	.702
J	Ethylbenzene	.402	.654	.459
,	datio	.589	.845	.332
1	rolys	1.908	0.427	3.388
	Formaldehyde	6.356	4.773	7.940
1	itrot	.738	1.758	1.719
J	4	1.309	.257	61
1	inyl Aceta	.694	8.700	0.688
1	Oxyacetylation	49.6944	8.700	0.688

TRE estimate is less than 3, a false Group 1 indication would have to be confirmed with actual testing. A tabular summary of this information is shown in Table 5.

Recommendations

An engineering estimate based TRE cut-off is a viable alternative to performance testing, with a TRE-cutoff equal to 3 for non-halogenated vents excuding high flow/low concentration vents and equal to 1.5 for halogenated vents.